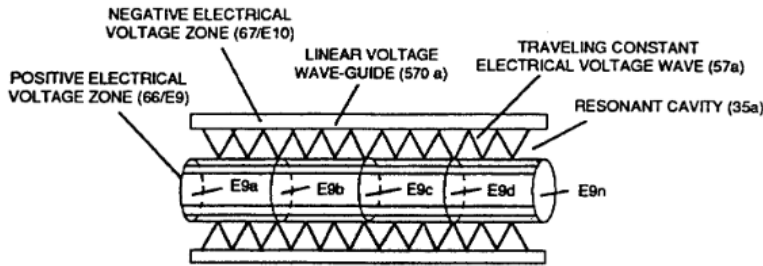


# 8-2 - Traveling Voltage Wave-Guides

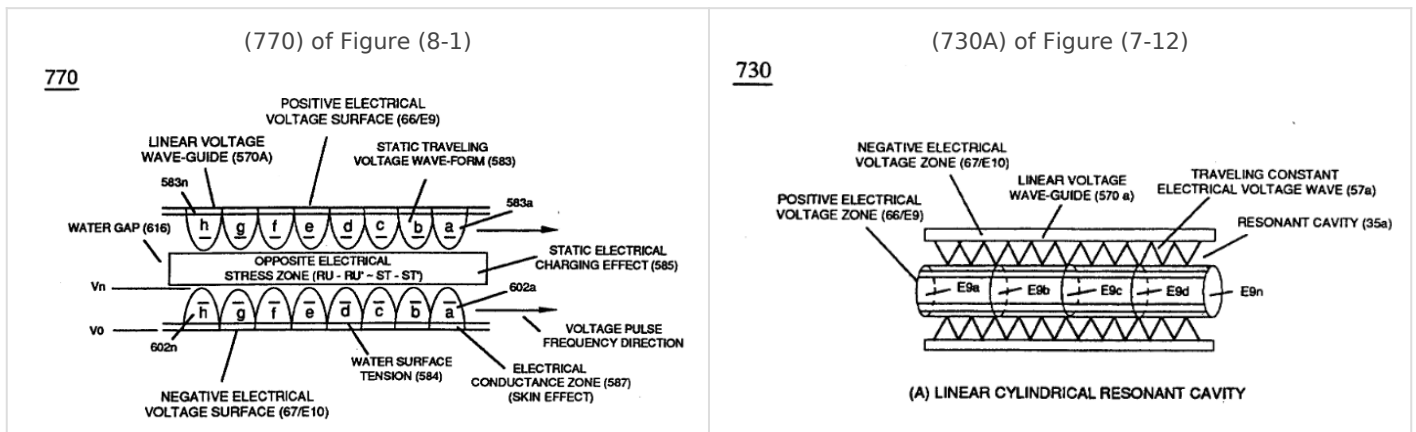
730

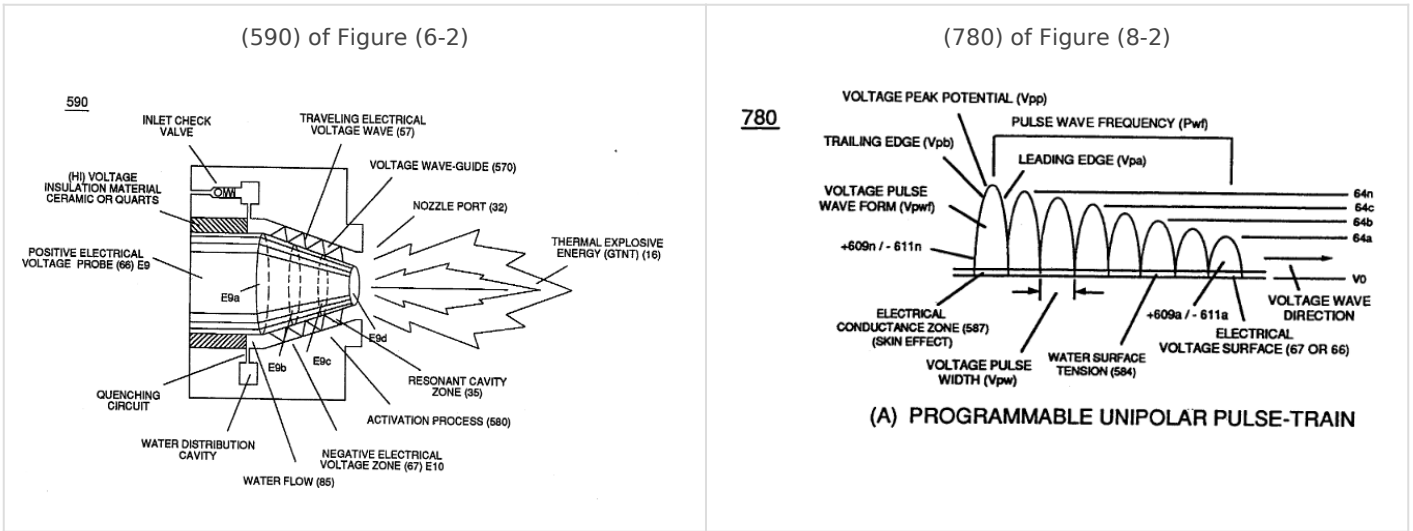


(A) LINEAR CYLINDRICAL RESONANT CAVITY

The formation of tubular **Traveling**

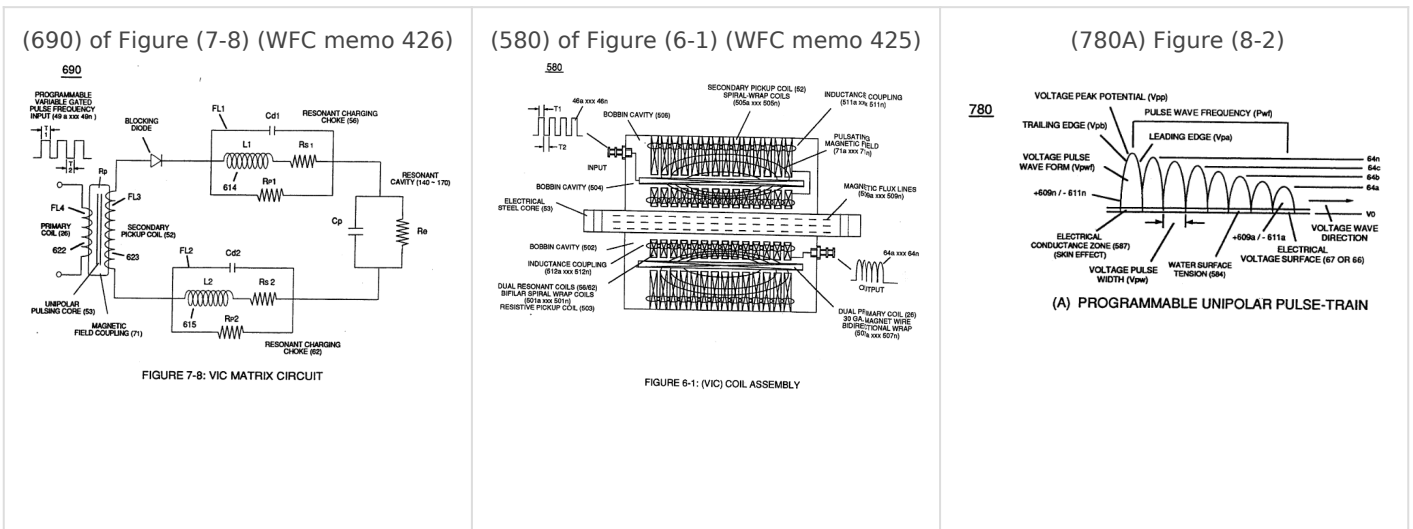
**Voltage Wave-guide** (570a) of Figure (7-12) (WFC Memo 426) as to (770) of Figure (8-1) is physically formed when **positive electrical voltage surface** (66/E9) and **negative electrical voltage surface** (67/E10) are placed in parallel space relationship to form voltage surfaces (E9/E10) about an cylindrical axis of rotation having space-gap (35) there between and thus, fanning **Cylindrical Resonant Cavity** (730A) of Figure (7-12) as to (770A) of Figure (8-1) when **space-gap** (616) of Figure (720) exposes **injected water bath** (85) to unipolar pulse-oscillation of high voltage intensity of **opposite polarity** (67/66) as to (780) of Figure (8-2) which, in turn, propagates **opposite electrical attraction force** (RR' \_ 88') of Figure (7-4), as illustrated in (590) of Figure (6-2) as to (585) of Figure (8-1).

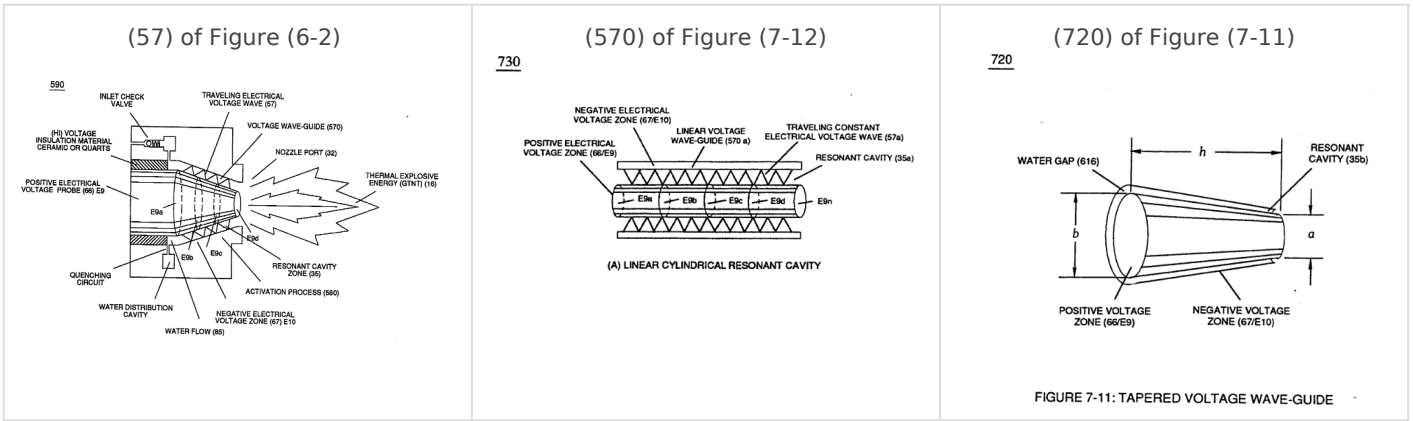




The dielectric property of water (85) (resistance to electron flow) in conjunction with **VIC Coil Matrix Circuit** (690) of Figure (7-8) (WFC memo 426) as to **VIC Coil Assembly** (580) of Figure (6-1) (WFC memo 425) ability to inhibit amp "influxing" (**Electron Bounce Phenomenon EbP**) during pulsing operations (49a xx 49n) allows voltage amplitude of pulse-frequency potential (T1a xxxT1n) as to (Vo -64a-64b -64c - Vn) of (780A) Figure (8-2) to be applied across cross-sectional circular-ring water bath (85) (donut shape) to cause **Voltage Wave-Form** (57) of Figure (6-2) to travel the entire longitudinal length of water-gap (616) since stainless steel material (s/s) (T304) forming Voltage surfaces (E9/E10) electrically conducts and transfers (**skin effect**) **Voltage Pulse-Frequency Potential** (583) along the inside surface area of the chemically inert and non-oxidizing stainless steel (s/s) tubular material (E9/E10) which physically dictates the shape and configuration of voltage waves (66/67)

... forming tubular voltage wave-guide (s) (570) of Figure (7-12) that, now, becomes the same physical configuration of **Water Gap** (616), as illustrated in (720) of Figure (7-11).





The surface tension of water (584) adjacent to both voltage surfaces (E9 / E10) further aids the transmission of voltage potential (66/67) since **Electrical Charging Effect (585)** of Figure (7-4) does not change or alter the dielectric value of water (Re).

650

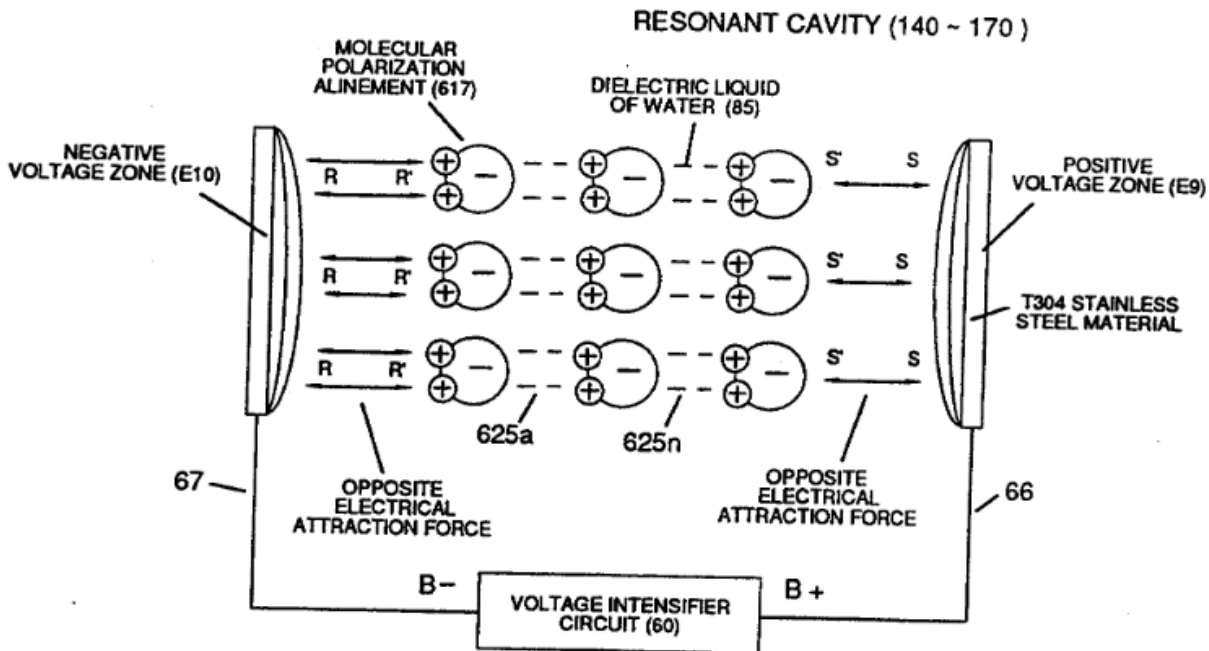


FIGURE 7-4: ELECTRICAL CHARGING EFFECT

Together, the **Voltage Coefficient of Water** ( $e/E_0$ ) of **Equation (Eq 21)** and the **Voltage Coefficient of the stainless steel** ( $s/s$ ) material fanning voltage surfaces (E9/E10), now, allows the establishment and performance of **Traveling Electrical Voltage Wave-Guide (583/602)** since electrical conductance zone (587) between electrical surface (S) (E9/E10) and the **dielectric surface tension of water (584)** acts and performs as an electrical conductor (Skin Effect)

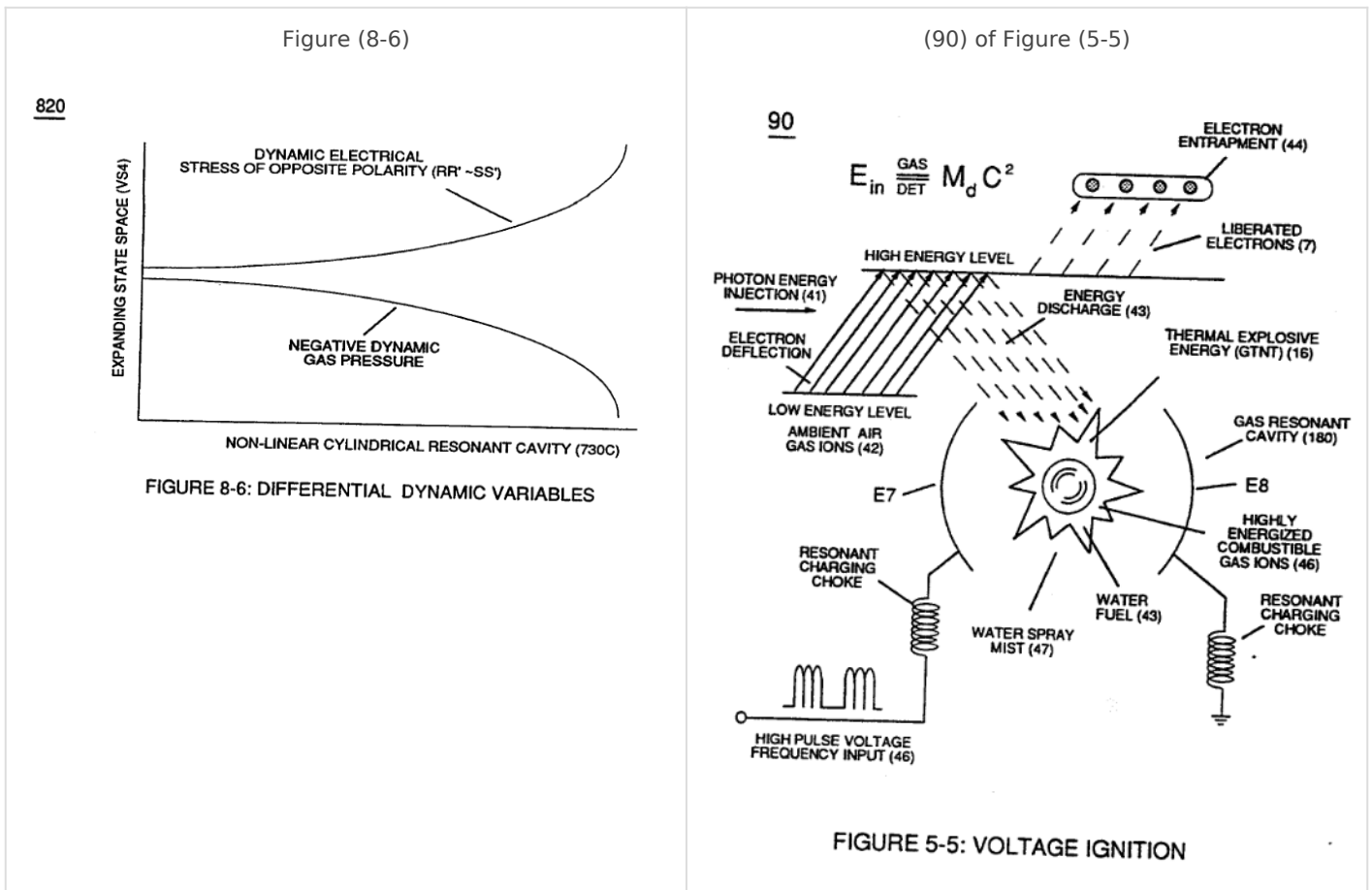
$$C = \frac{0.2249 e A}{d E_0} \text{ Picofarads}$$

... since electrical transmission zone (587) is almost free of electron leakage

...since **Water Bath** (85) is a dielectric-liquid (typically 78.54Q) that does not like to transfer nor exchange electrons

... thereby, maintaining **voltage amplitude potential** ( $V_0 - 64a - 64b - 64c - V_n$ ) of Figure (8-6) without experiencing amp arc-over across **Water-Gap** (616) in any appreciable amount

... allowing pulsating opposite electrical attraction forces ( $RR' / SS'$ ) to perform the work of "**Electrically Charging**" water bath (85) to bring-on and trigger **Hydrogen Fracturing Process** (90) of Figure (5-5), as illustrated in **Energy Pumping stage** (520) of Figure (5-3).



(520) of Figure (5-3)

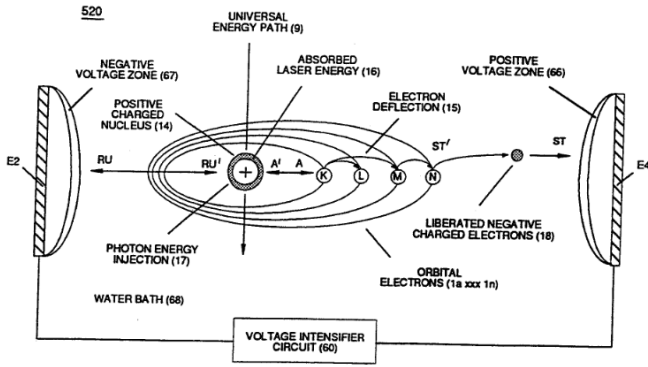


FIGURE 5-3: ENERGY PUMPING ACTION

**Voltage Intensifier Matrix Circuit (690)** of Figure (7-8) electrically connected with resistive liquid (85/Re) (forming **Resonant Water Gap "Cp"** of Figure 7-8) propagates the transmission of **Traveling Voltage Wave-Form (57)** of Figure (6-2) as to (770) of Figure(8-1) by the functional relationship of **Circuit Resistance Equation (Eq 9)** during programmable **Voltage Pulsing** operations (49a xxx 1'3 xxx 49n) of Figure (8-2).

(690) of Figure (7-8)

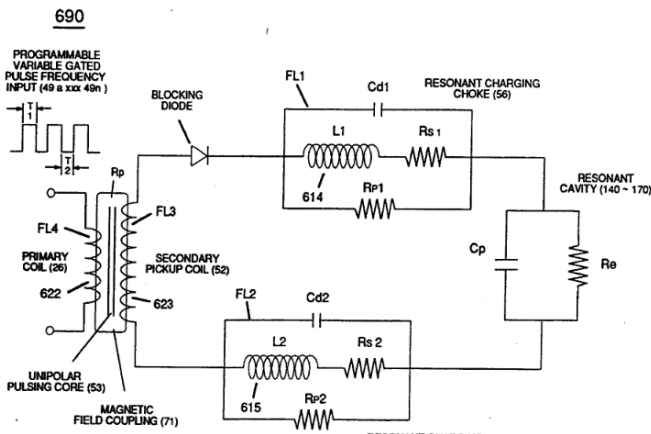
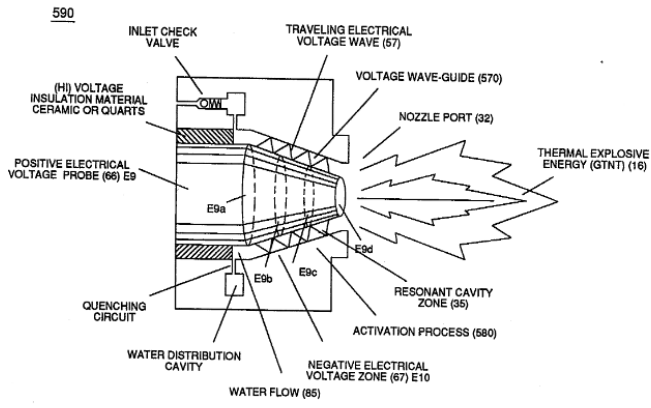


FIGURE 7-8: VIC MATRIX CIRCUIT

Circuit Resistance Equation (Eq 9)

$$Z = R_I + Z_2 + Z_3 + R_E$$

(57) of Figure (6-2)



(770) of Figure(8-1)

770

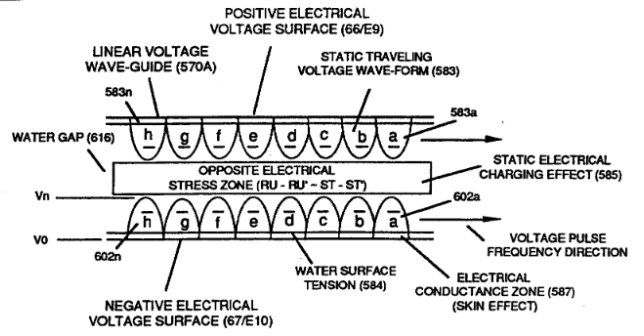
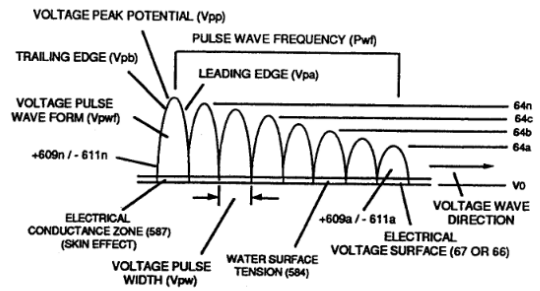


Figure (8-2)

780



(A) PROGRAMMABLE UNIPOLAR PULSE-TRAIN

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