

# Capacitance Reactance

**Capacitance Reactance** is determined by the insulation resistance ( $R_s+R_e$ ) and **Inductance** ( $L1/L2$ ) interacting together during D.C. Pulsing.

Dielectric property of water opposes amp leakage ( $R_e$ ) while another property of water takes-on an "**Electrical Charge**".

Water temperature ( $R_t$ ) (cool-to-the-touch) keeps ( $R_e$ ) constant since amp flow remains minimal.

**Plate Inductance** ( $L_c$ ) is **Inductance Reactance** of **Inductor** ( $L1$ ) and **Inductance Reactance** of **Inductor** ( $L2$ ) in series with **Resonant Capacitor** (140 -170) of Figure (7-6) as to (690) of Figure (7-8).

Resonant Capacitor (140 -170) of Figure (7-6)

670

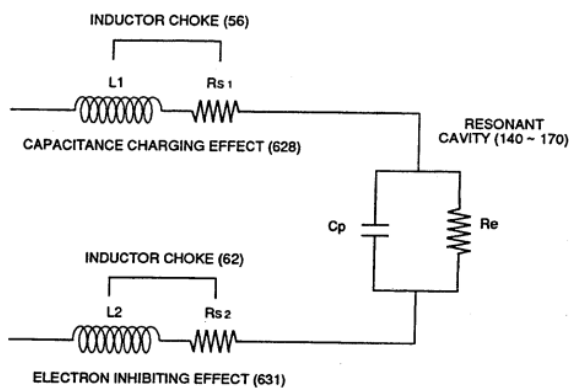


FIGURE 7-6: RESONANT VOLTAGE EFFECT

(690) of Figure (7-8)

690

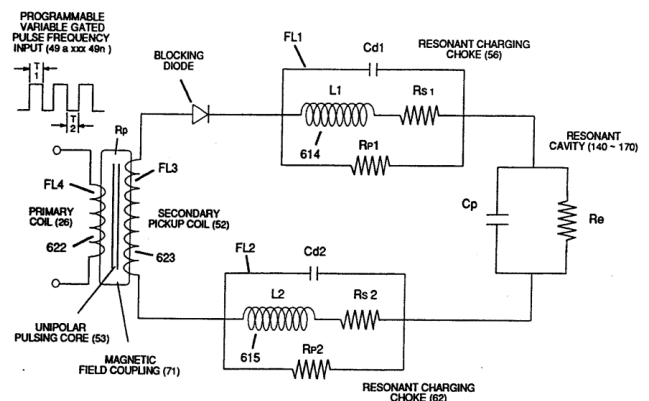


FIGURE 7-8: VIC MATRIX CIRCUIT

In terms of **Component Reactance**, Inductors ( $L1/L2$ ) should always be larger than **Capacitor** ( $R_e$ ) of Figure (7-2) in order to maximize amp restriction to enhance "**Voltage Deflection**" ( $SS' - 617a \text{ xxx } 617n - RR'$ ) of Figure (7-4) and, is expressed by :

Capacitor (ER) of Figure (7-2)

630

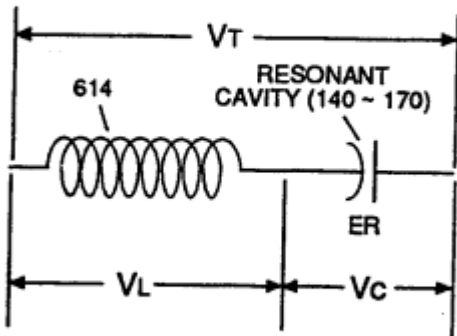
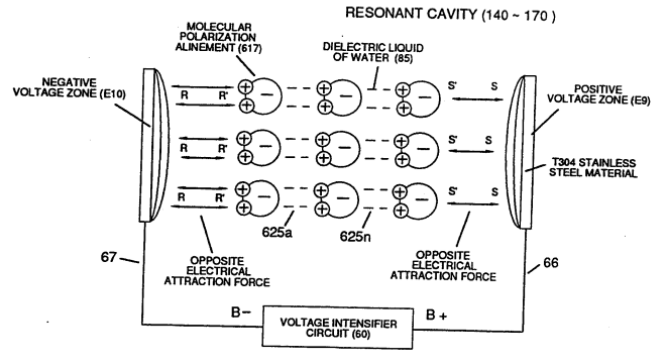


FIGURE 7-2: LC CIRCUIT

"Voltage Deflection" of Figure (7-4)

650



(Eq 24)

$$Z = X_L - X_C$$

Whereas,

**Capacitor (ER)** should remain relatively small due to the dielectric value of water to obtain maximum **Thermal Explosive Energy-Yield** (16a xxx 16n) of Figure (4-5) and subsequently establishing **Quenching Circuit** (370) of Figure (3-40) to prevent gas ignition inside traveling voltage wave-guide (590) of Figure (6-2) as to (730) of Figure (7-12)

Quenching Circuit (370) of Figure (3-40)

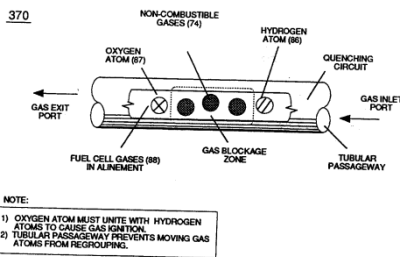
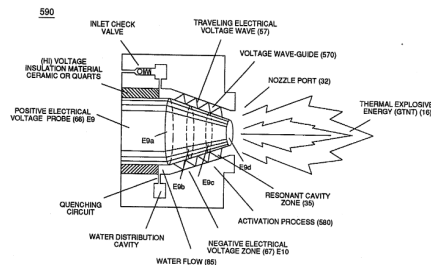
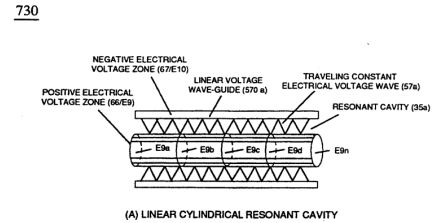


FIGURE 3-40: QUENCHING ACTION

(590) of Figure (6-2)



(730) of Figure (7-12)



... to bring-on and trigger Hydrogen Fracturing Process (390) of Figure (3-42) once liberated and expanding water gases (100) of Figure (4-8) passes beyond exit port (E9d)

(390) of Figure (3-42)

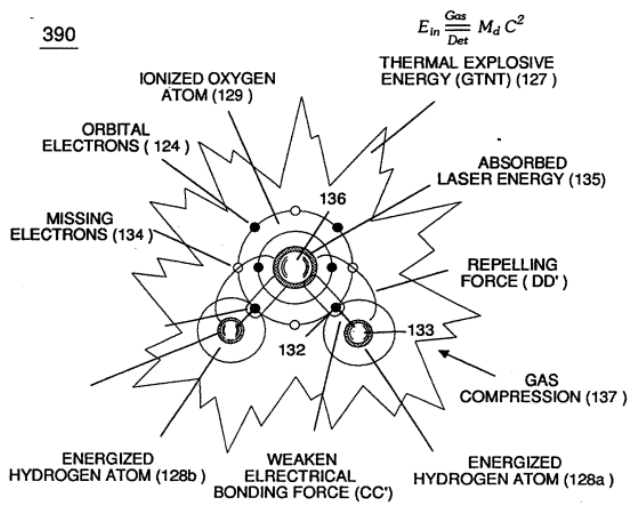


FIGURE 3-42: HYDROGEN FRACTURING PROCESS

(100) of Figure (4-8)

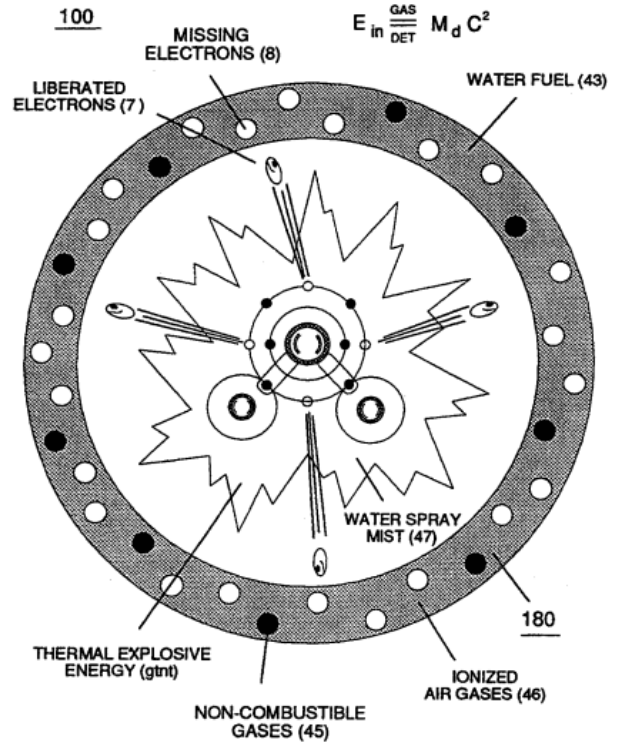


FIGURE 4-8: GAS IGNITION STAGE

... activating Voltage Ignition Process (90) of Figure (5-5)

(90) of Figure (5-5)

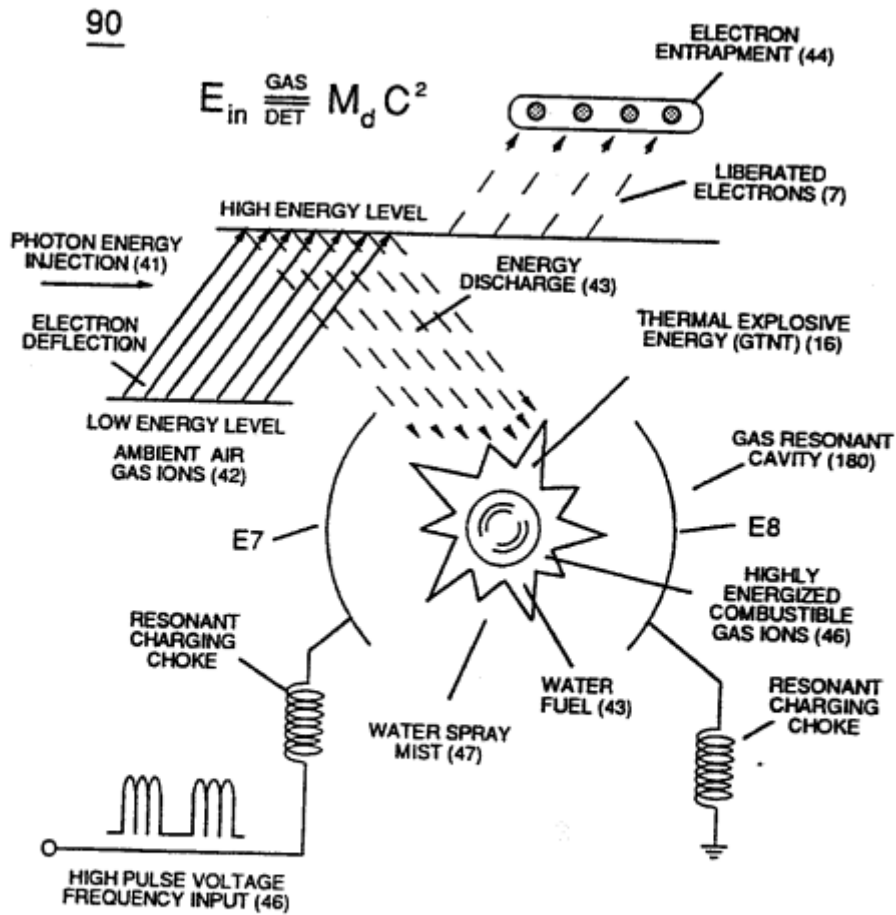


FIGURE 5-5: VOLTAGE IGNITION

... utilizing **Dynamic Voltage Potential** (600) of Figure (6-3) of opposite electrical stress (SS' - 617 - RR') to cause **thermal atomic agitation** (90) of Figure (4-7) (kinetic heat by atomic motion)

(600) of Figure (6-3)

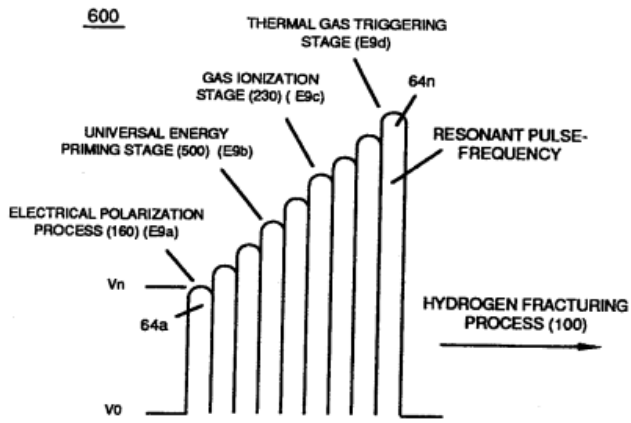


FIGURE 6-3: DYNAMIC VOLTAGE POTENTIAL

(90) of Figure (4-7)

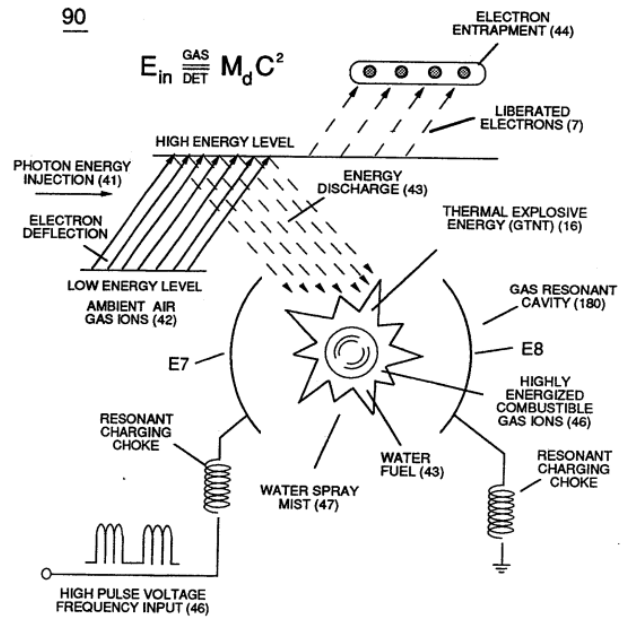


FIGURE 4-7: VOLTAGE IGNITER STAGE

which, when occurring at **gas exit port** (32) of Figure (4-5), spark-ignites expanding water gas-fuel (45/46/47) of Figure (4-5) during water inject cycle (70) of Figure (4-5)

Figure (4-5)

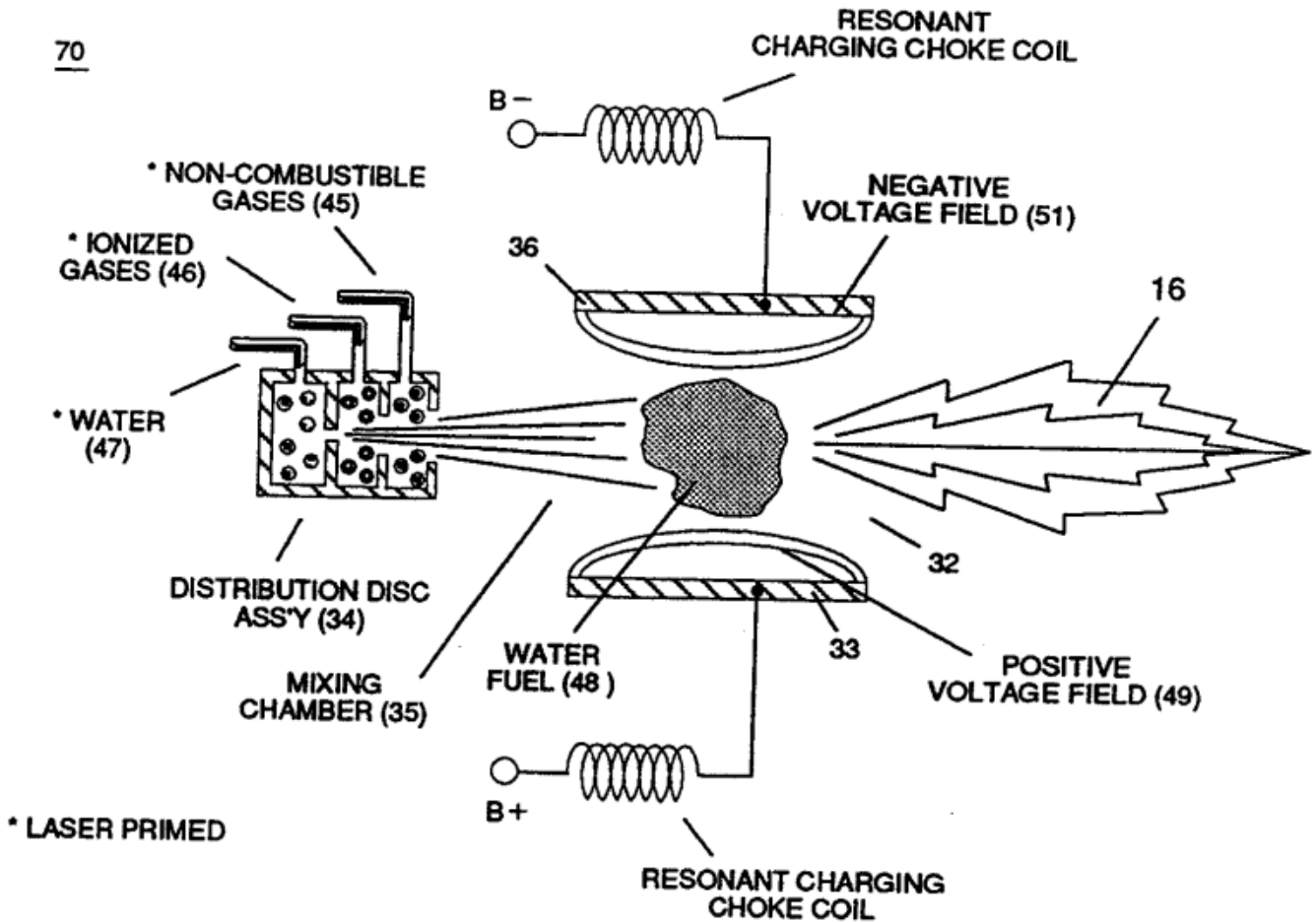


FIGURE 4-5: VOLTAGE TRIGGERING

... releasing thermal explosive energy (gtnt) (16) under control state.

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