Capacitance Reactance

Capacitance Reactance is determined by the insulation resistance (Rs+Re) and **Inductance** (L1/L2) interacting together during D.C. Pulsing.

Dielectric property of water opposes amp leakage (Re) while another property of water takes-on an "**Electrical Charge**".

Water temperature (Rt) (cool-to-the-touch) keeps (Re) constant since amp flow remains minimal.

Plate Inductance (Lc) is **Inductance Reactance** of **Inductor** (L1) and **Inductance Reactance** of **Inductor** (L2) in series with **Resonant Capacitor** (140 -170) of Figure (7-6) as to (690) of Figure (7-8).

Resonant Capacitor (140 -170) of Figure (7-6)
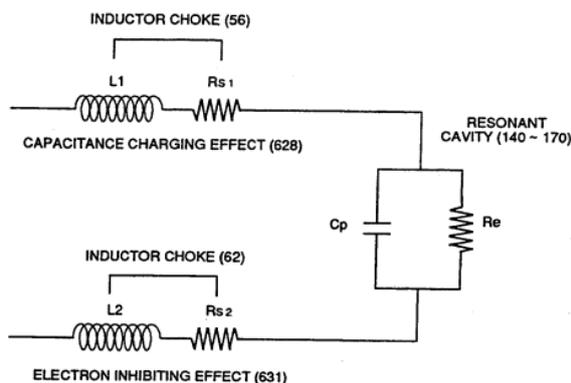

FIGURE 7-6: RESONANT VOLTAGE EFFECT

(690) of Figure (7-8)
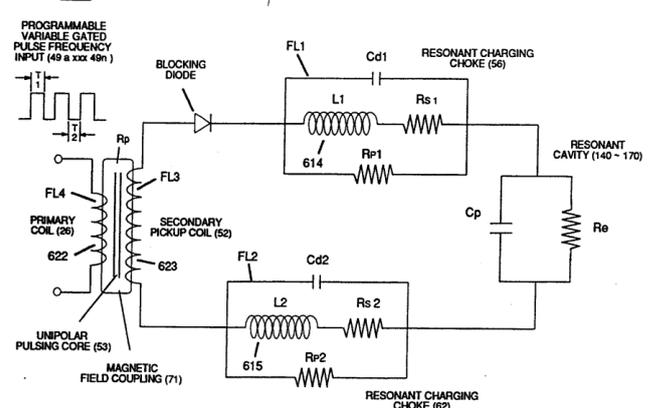
FIGURE 7-8: VIC MATRIX CIRCUIT

In terms of **Component Reactance**, Inductors (L1/L2) should always be larger than **Capacitor** (ER) of Figure (7-2) in order to maximize amp restriction to enhance "**Voltage Deflection**" (SS' - 617a xxx 617n - RR') of Figure (7-4) and, is expressed by :

| **Capacitor** (ER) of Figure (7-2)	"**Voltage Deflection**" of Figure (7-4)

630
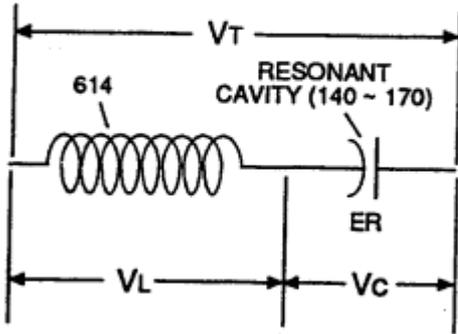
FIGURE 7-2: LC CIRCUIT

650
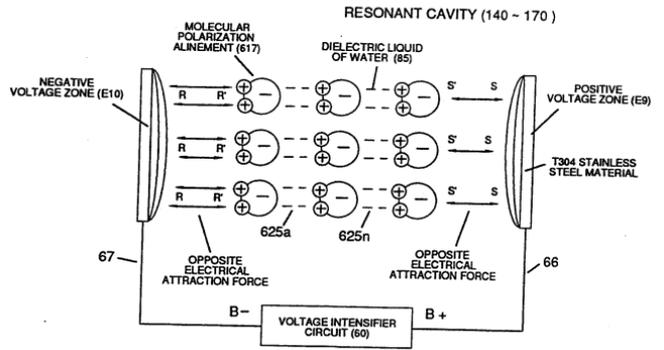
(Eq 24)

$$Z = X_L - X_C$$

Whereas,

Capacitor (ER) should remain relatively small due to the dielectric value of water to obtain maximum **Thermal Explosive Energy-Yield** (16a xxx 16n) of Figure (4-5) and subsequently establishing **Quenching Circuit** (370) of Figure (3-40) to prevent gas ignition inside traveling voltage wave-guide (590) of Figure (6-2) as to (730) of Figure (7-12)

Quenching Circuit (370) of Figure (3-40)	(590) of Figure (6-2)	(730) of Figure (7-12)

370
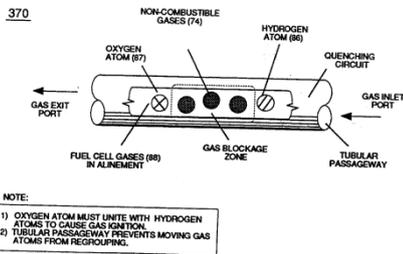
FIGURE 3-40: QUENCHING ACTION

590

730

(A) LINEAR CYLINDRICAL RESONANT CAVITY
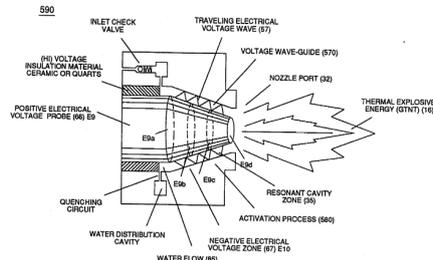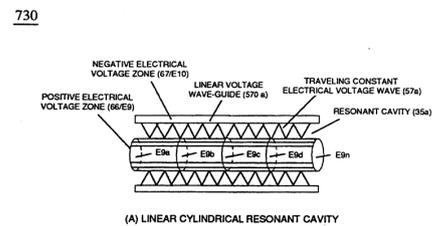
... to bring-on and trigger Hydrogen Fracturing Process (390) of Figure (3-42) once liberated and expanding water gases (100) of Figure (4-8) passes beyond exit port (E9d)
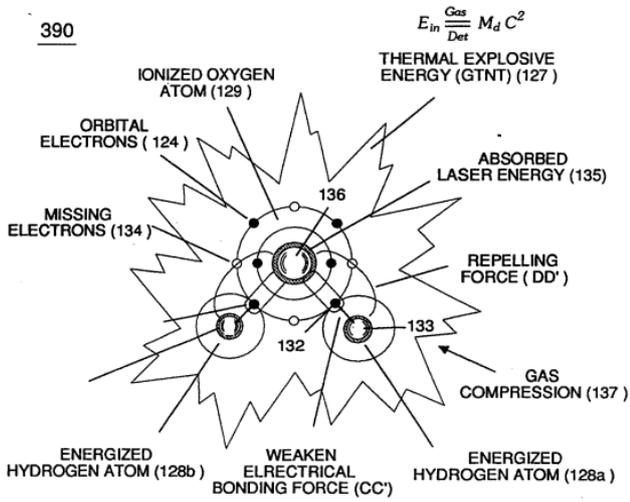
FIGURE 3-42: HYDROGEN FRACTURING PROCESS
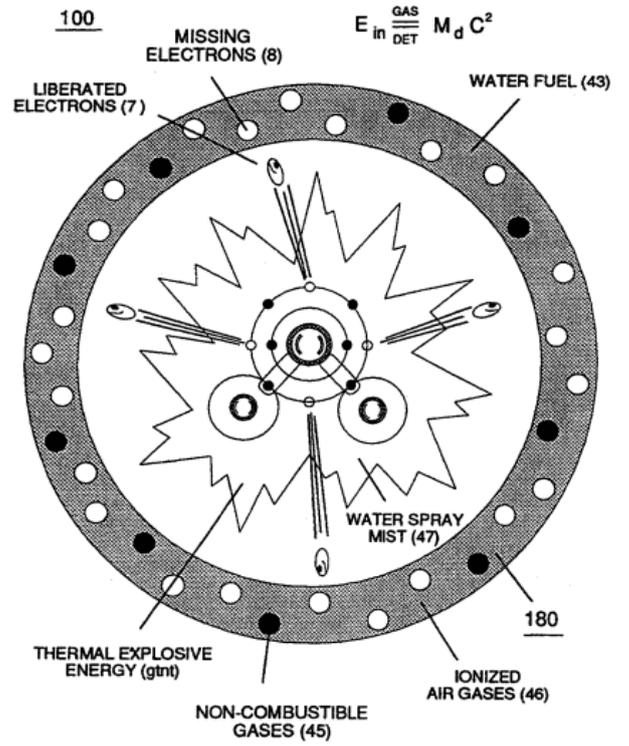
FIGURE 4-8: GAS IGNITION STAGE

... activating Voltage Ignition Process (90) of Figure (5-5)

90

$$E_{in} \overset{GAS}{\underset{DET}{=\!=}} M_d C^2$$

ELECTRON
ENTRAPMENT (44)

LIBERATED
ELECTRONS (7)

HIGH ENERGY LEVEL

PHOTON ENERGY
INJECTION (41)

ENERGY
DISCHARGE (43)

ELECTRON
DEFLECTION

THERMAL EXPLOSIVE
ENERGY (GTNT) (16)

LOW ENERGY LEVEL
AMBIENT AIR
GAS IONS (42)

GAS RESONANT
CAVITY (180)

E7

E8

HIGHLY
ENERGIZED
COMBUSTIBLE
GAS IONS (46)

RESONANT
CHARGING
CHOKE

WATER
FUEL (43)

RESONANT
CHARGING
CHOKE

WATER SPRAY
MIST (47)

HIGH PULSE VOLTAGE
FREQUENCY INPUT (46)

FIGURE 5-5: VOLTAGE IGNITION

... utilizing **Dynamic Voltage Potential** (600) of Figure (6-3) of <u>opposite electrical stress</u> (SS' - 617 - RR') to cause **thermal atomic agitation** (90) of Figure (4-7) (kinetic heat by atomic motion)

600

ELECTRICAL POLARIZATION
PROCESS (160) (E9a)

UNIVERSAL ENERGY
PRIMING STAGE (500) (E9b)

GAS IONIZATION
STAGE (230) (E9c)

THERMAL GAS TRIGGERING
STAGE (E9d)

64n

RESONANT PULSE-
FREQUENCY

Vn

64a

HYDROGEN FRACTURING
PROCESS (100)

V0
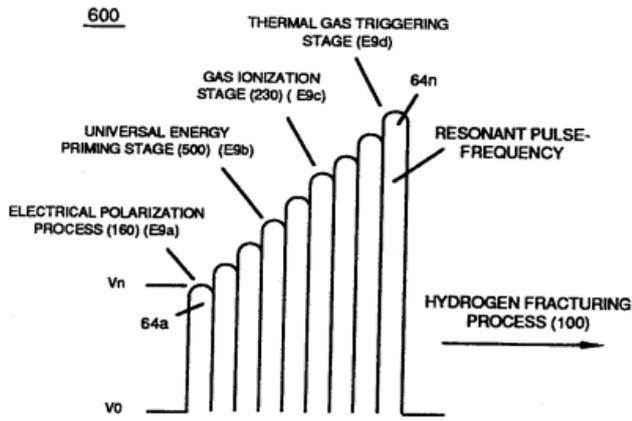
FIGURE 6-3: DYNAMIC VOLTAGE POTENTIAL

90

$$E_{in} \overset{GAS}{\underset{DET}{\equiv\!\equiv}} M_d C^2$$

ELECTRON
ENTRAPMENT (44)

LIBERATED
ELECTRONS (7)

HIGH ENERGY LEVEL

PHOTON ENERGY
INJECTION (41)

ENERGY
DISCHARGE (43)

ELECTRON
DEFLECTION

THERMAL EXPLOSIVE
ENERGY (GTNT) (16)

LOW ENERGY LEVEL
AMBIENT AIR
GAS IONS (42)

GAS RESONANT
CAVITY (180)

E7

E8

RESONANT
CHARGING
CHOKE

HIGHLY
ENERGIZED
COMBUSTIBLE
GAS IONS (46)

WATER
FUEL (43)

RESONANT
CHARGING
CHOKE

WATER SPRAY
MIST (47)

HIGH PULSE VOLTAGE
FREQUENCY INPUT (46)

FIGURE 4-7: VOLTAGE IGNITER STAGE

which, when occurring at **gas exit port** (32) of Figure (4-5), spark-ignites expanding water gas-fuel (45/46/47) of Figure (4-5) during water inject cycle (70) of Figure (4-5)

Figure (4-5)
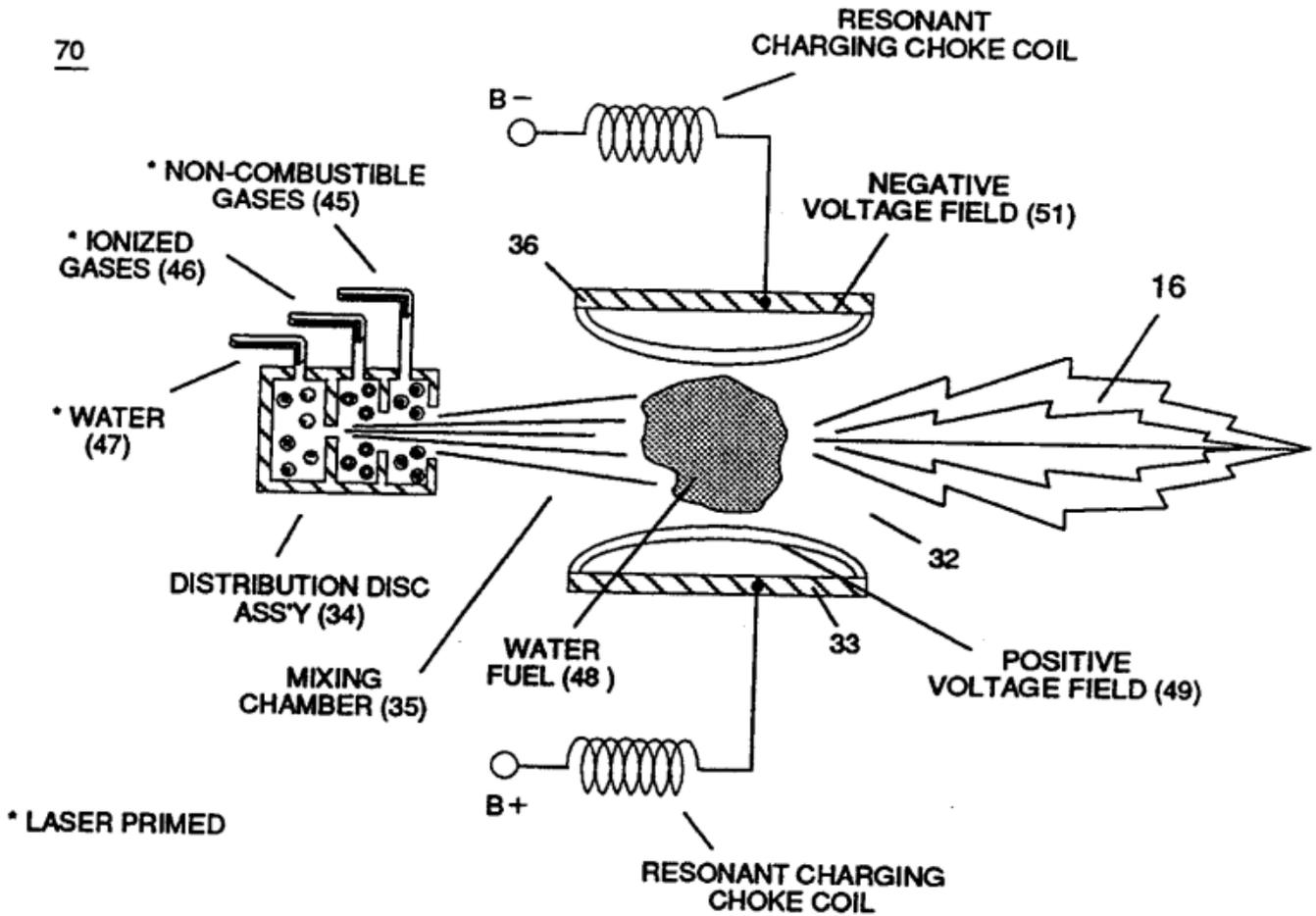
FIGURE 4-5: VOLTAGE TRIGGERING

... releasing thermal explosive energy (gtnt) (16) under control state.

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