

# Instant Explosion of Water

The "mode-of-operability" of **VIC Coil Assembly** allows **Voltage Potential** of opposite voltage polarity to increase and be attenuated up to and beyond 20 Kilovolts while inhibiting and restricting amp leakage in the milliamperes range ... establishing operational parameter of utilizing "**Opposite Electrical Attraction Force**" of "high voltage intensity" to "instantly" releases thermal explosive energy (gtnt) from natural water.

The **Voltage Intensifier Circuit** takes advantage of the "**Electron Bounce Phenomenon**" to trigger **Hydrogen Fracturing Process** without amp influxing. **Taper Resonant Cavity** functions as a "**Voltage Amplifier**" when interlinked with **VIC Circuit**.

**Voltage Intensifier Circuit** (60) of Figure (3-22) (Memo WFC 422 DA) as to Figure (1-1) (Memo WFC 420) and **Voltage Intensifier Circuit** (620) of Figure (7-1) are specifically designed to restrict amp flow during **Programmable Pulsing Operations** (49a xxx 49n) but in different operational modes:

Voltage Intensifier Circuit (60) of Figure (3-22)

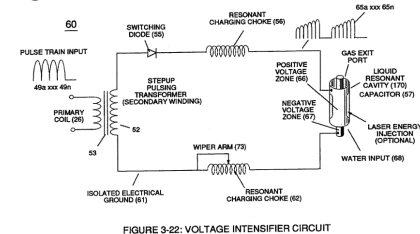


FIGURE 3-22: VOLTAGE INTENSIFIER CIRCUIT

Figure (1-1) (Memo WFC 420)

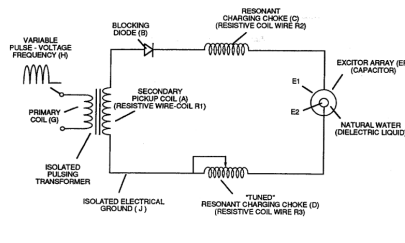


FIGURE 1-1: VOLTAGE INTENSIFIER CIRCUIT (AA)

Voltage Intensifier Circuit (620) of Figure (7-1)

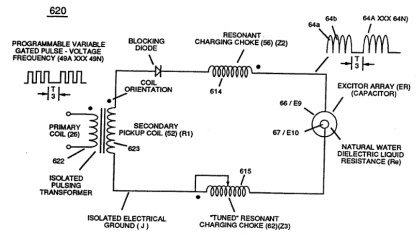


FIGURE 7-1: VIC IMPEDANCE NETWORK

VIC voltage circuit (60) utilizes copper wire-wrap to form **Resonant Charging Chokes** (56/62) of Figure (3-22) in conjunction with **Switching Diode** (55) to encourage and make use of "**Electron Bounce**" phenomena (700) of Figure (7-9) to help promote **Step Charging Effect** (628) of Figure (7-7) by preventing electrical discharge of **Resonant Cavity** (140 - 170) since **Blocking Diode** functions as an "**Open**" switch during **Pulse Off-time**;

(56/62) of Figure (3-22)

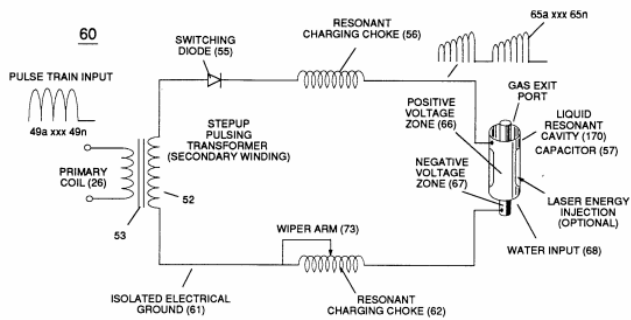


FIGURE 3-22: VOLTAGE INTENSIFIER CIRCUIT

(700) of Figure (7-9)

700

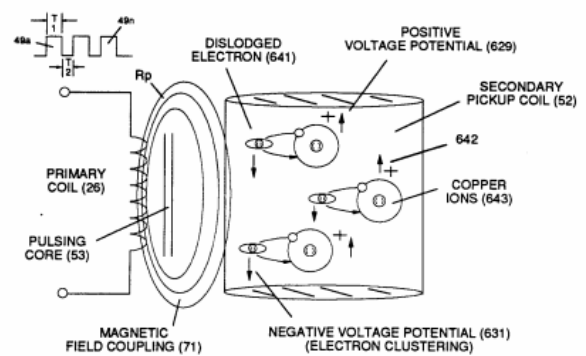


FIGURE 7-9: ELECTRON BOUNCE PHENOMENON (EbP)

(628) of Figure (7-7)

680

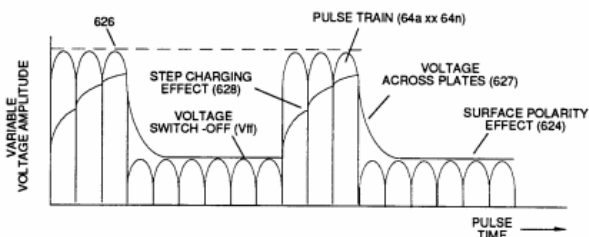


FIGURE 7-7: VOLTAGE CHARGING EFFECT

whereas,

**VIC Voltage Enhancement Circuit** (VIC - VB) (620) of Figure (7-1) incorporates the use of **stainless steel wire-wrap coils** (614/615) to accomplish the formation of unipolar gated pulse-wave (64a xxx T3 xxx 64n) without experiencing "signal distortion" or "signal degradation" (preventing transformer ringing during signal propagation) as elevated voltage levels ( - xx Vc- xx Vd - xx Vn) while allowing the reduction of **Capacitor-Gap** (Cp) (616) of Figure (7-11) width spacing (57 of Figure 3- 25 ~35 of Figure 6-2) (typically .060 - .010) respectively as illustrated in **Tubular Resonant Cavity** (170) as to **Taper Resonant Cavity** (620) of Figure (7-1).

(VIC - VB) (620) of Figure (7-1)

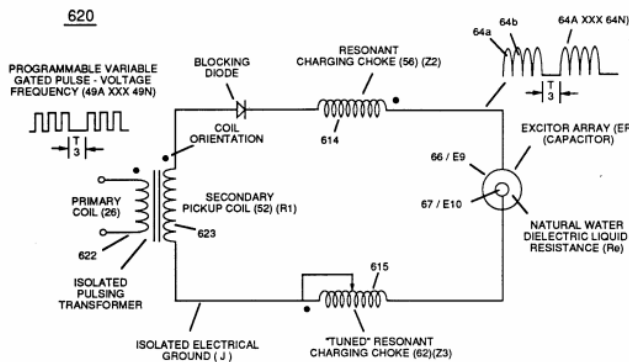


FIGURE 7-1: VIC IMPEDANCE NETWORK

(616) of Figure (7-11)

720

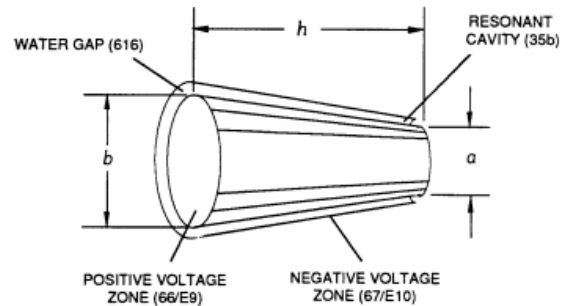


FIGURE 7-11: TAPERED VOLTAGE WAVE-GUIDE

(57 of Figure 3- 25 ~35 of Figure 6-2)

170

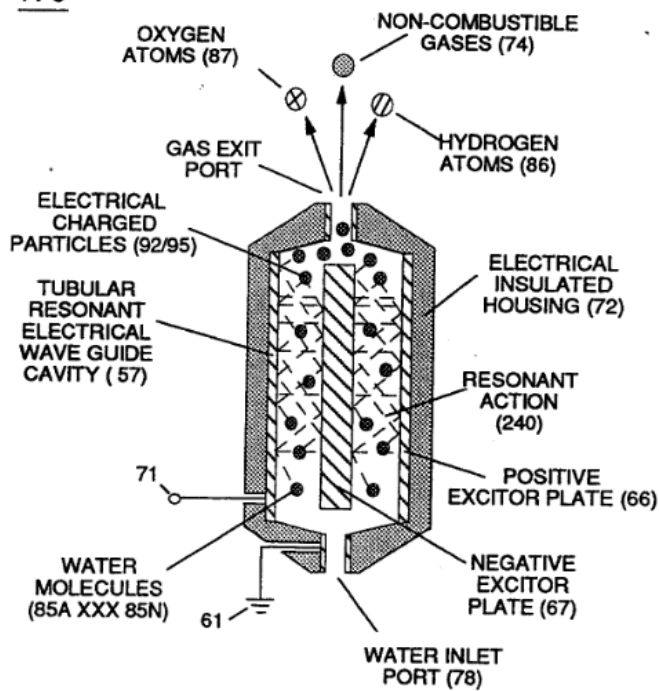


FIGURE 3-25: RESONANT CAVITY

**Switching Diode** (55) of Figure (3-22) prevents Bidirectional electron flow (current flow in one direction only) since **Blocking Diode** (55) only conducts "current flow" in the direction of schematic-arrow while being placed in-line with **VIC Circuit** impedance interaction ( $R1 + Z2 + Z3 + Re$ ), as mathematically extrapolated in **Circuit Equation** (Eq 9)

(55) of Figure (3-22)

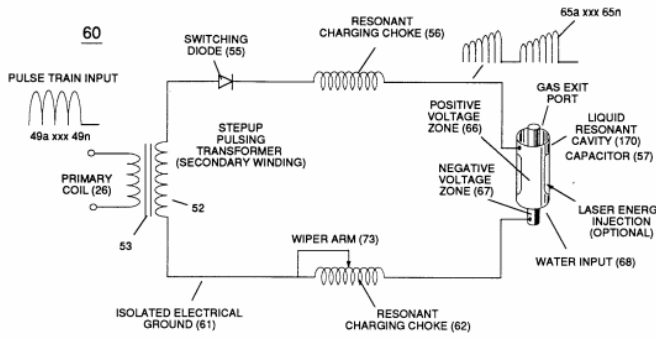


FIGURE 3-22: VOLTAGE INTENSIFIER CIRCUIT

(Eq 9)

$$Z = R_I + Z_2 + Z_3 + R_E$$

... **Diode** (55) being placed between **Secondary Pickup Coil** (52) and **Resonant Charging Choke** (56) to act as an electronic switch in open-position during pulse off-time (**T2**) of Figure (7-8) while preventing electron flow in reverse direction when **Inductor** (L1) **collapsing electromagnetic field** (FL1) produces another **unipolar pulse wave-form** (64a - 64b).

(T2) of Figure (7-8)

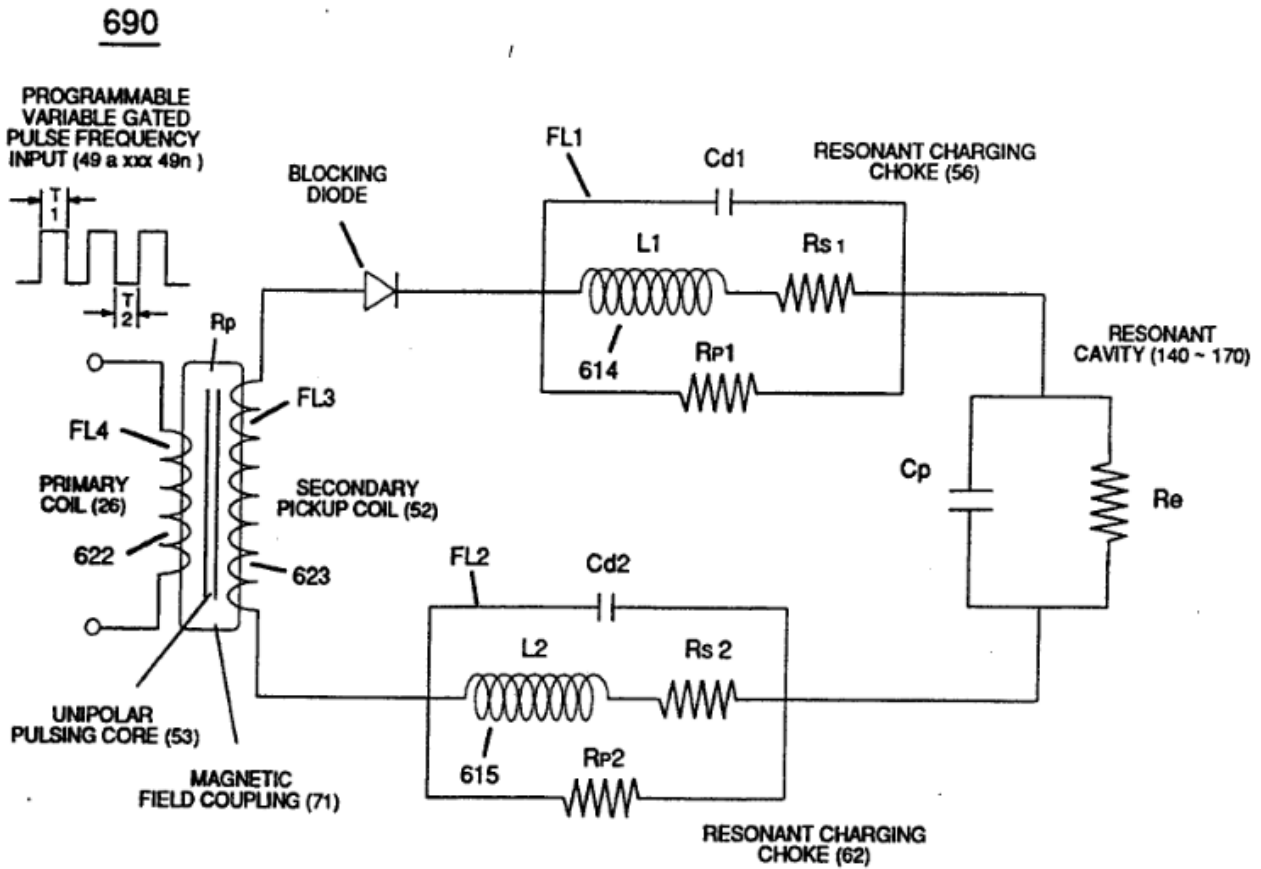


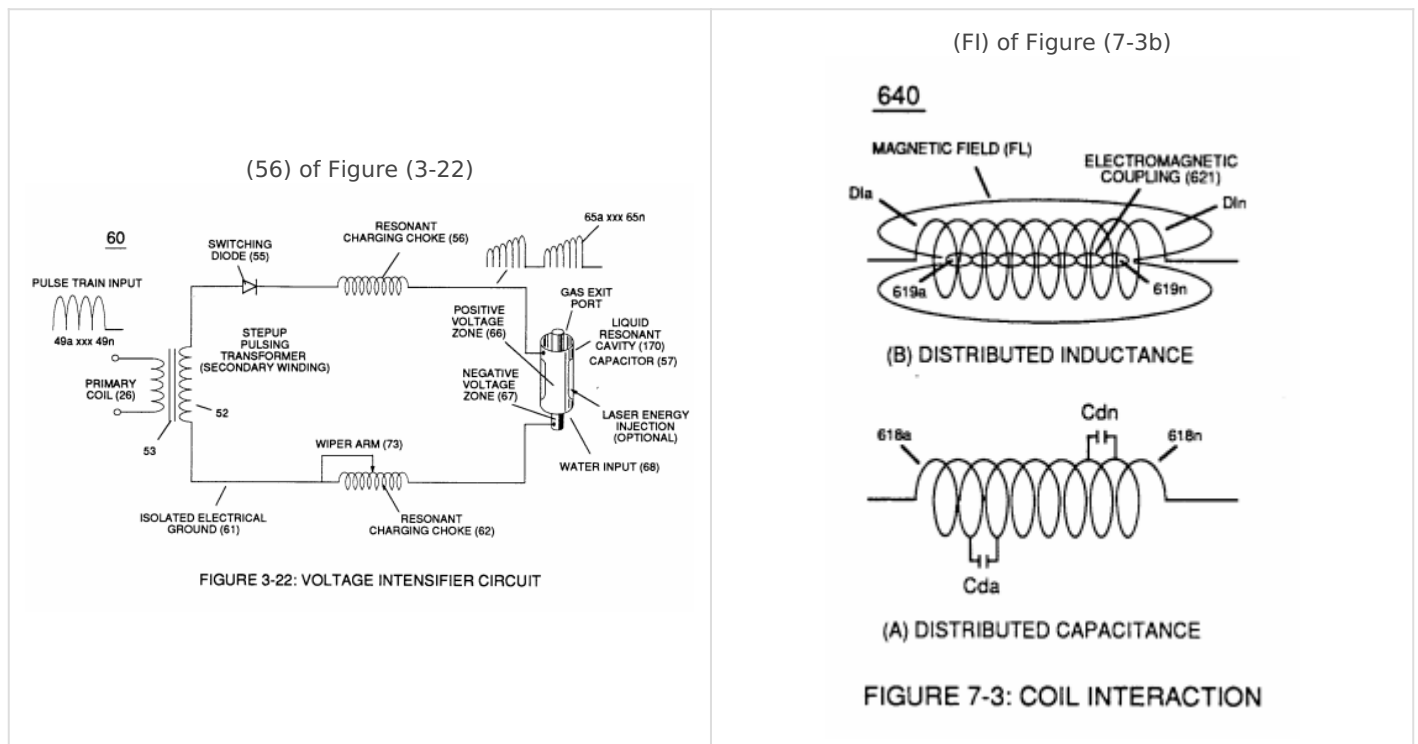
FIGURE 7-8: VIC MATRIX CIRCUIT

... producing **unipolar voltage wave-form** (64a xxx 64n) during repeated pulse-signal (46a xxx 46n) on-time (T1a xxx T1n)

... allowing the formation of an gated pulse-frequency pulse-train (64a/64b - T3 - 64a/64b) when pulse off-time (T3) is greater than time-period (T2)

... input-signal (49a xxx 49n) being a **Pulse-Train** where (T2) **pulse offtime** (T2) is adjusted to allow **Unipolar Pulse-Train** (64a xxx T3 xxx 64n)

... outputting **Voltage-wave signal** (64a xxx 64n) being a pulse-frequency doubler due to **Inductance Reactance** (FL) of **Inductor Coil** (56) of Figure (3-22) when collapsing magnetic field (FL) of Figure (7-3b) re-cuts **coil-wrap** (LI) during each pulse off-time (T2)



... producing a second **unipolar voltage wave-form** (64b) during the rise and fall of **magnetic field** (71), as further illustrated in (620) of Figure (7-1)

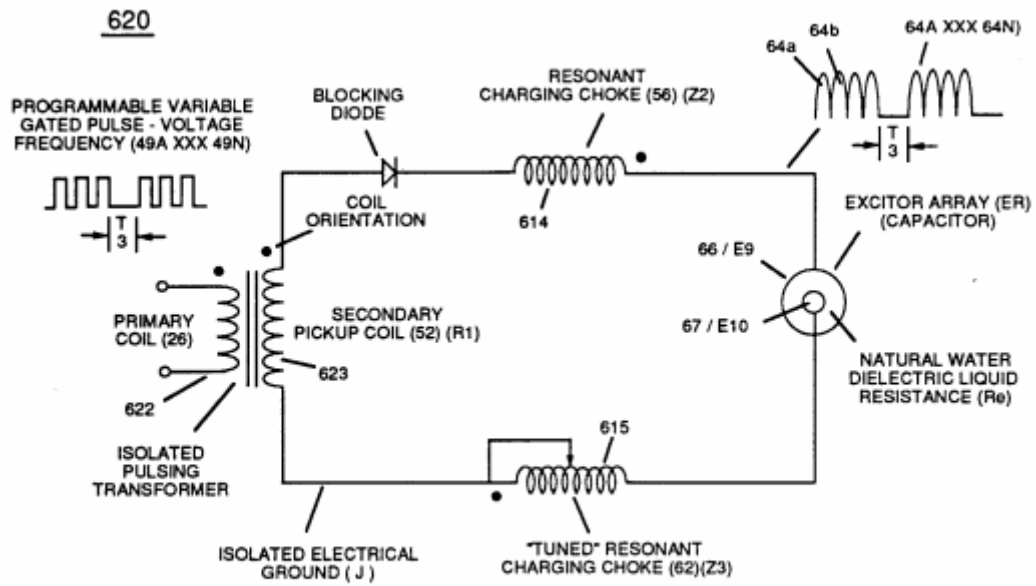


FIGURE 7-1: VIC IMPEDANCE NETWORK

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