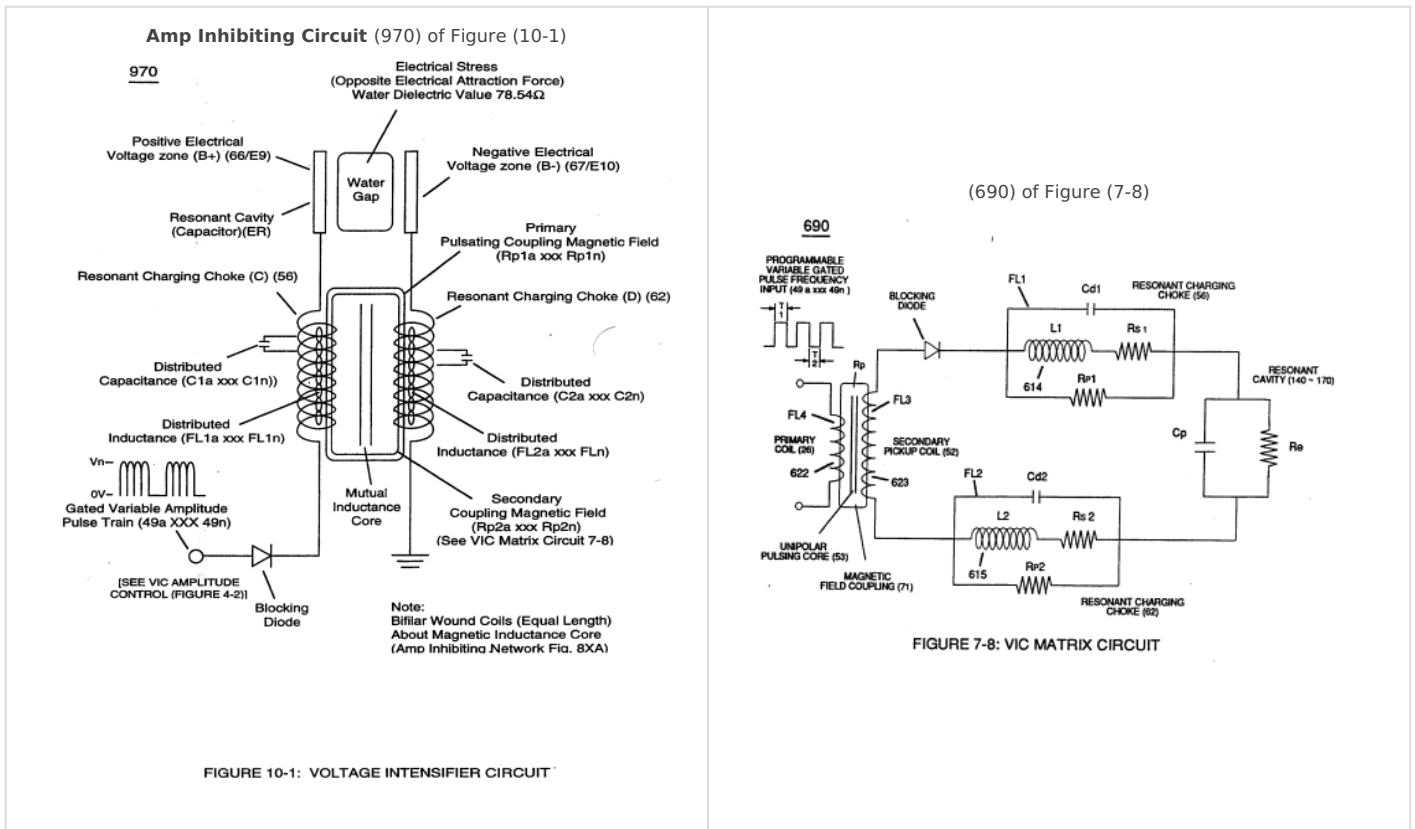


Propagating Electrical Stress

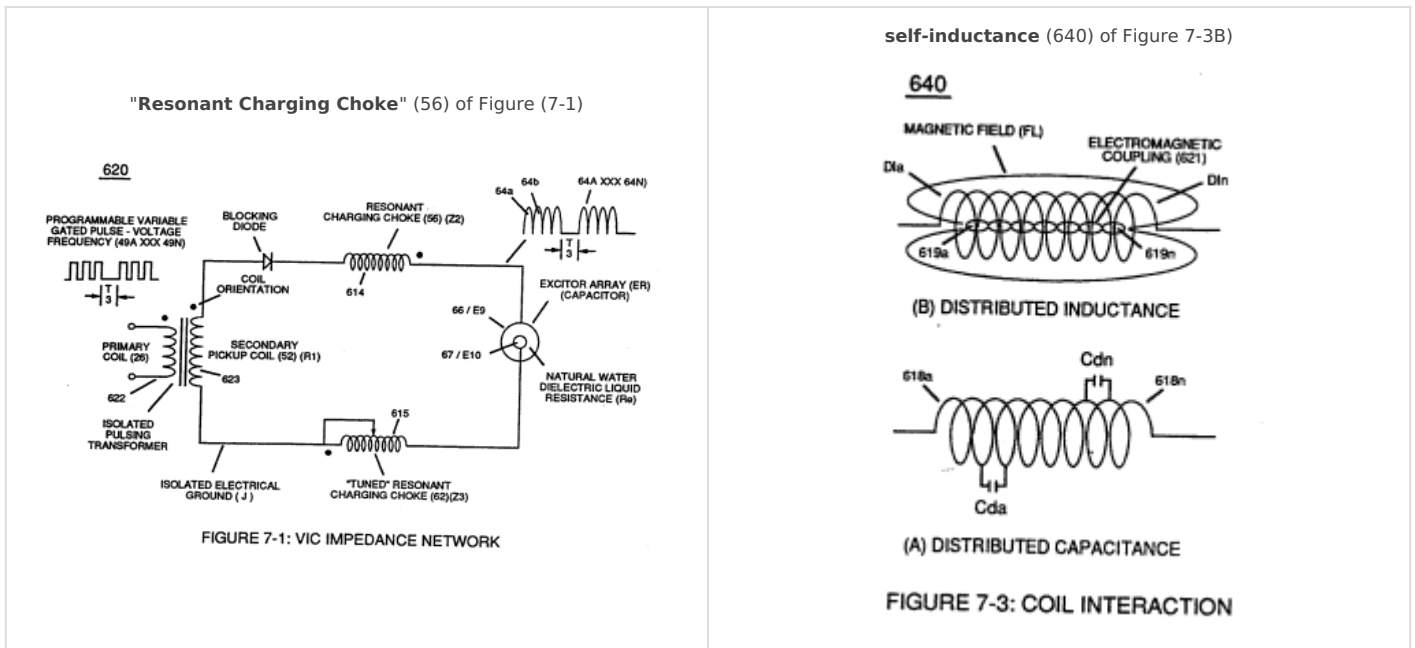
As in reference to **WFC Patent Validation Report** dated January 14, 1983 as per **WFC Test-Results** "Mode of Operability" of using "**Voltage Potential**" to "**Dissociates the Water Molecule**" by way of the "**Electrical Polarization Process**" (160) of Figure (3-26) as so specified under U.S. Patent Law (35 USC 101) demonstrate operability, the applied **Pulse-Voltage Frequency** is adjusted to tune-in to the dielectric properties of water by the use of WFC "**Amp Inhibiting Circuit**" (970) of Figure (10-1), as further illustrated in **WFC Tech-Brief** titled "**The Birth of New Technology**"

... U.S. Patent Memos 420 - 428, including "Table of Tabulation" (Appendix A) as to "Glossary of Application Notes" (Appendix B).

The **Amp Inhibiting Circuit** (970) of Figure (10-1) as to (690) of Figure (7-8) is composed of two copper wires "**Bifilar**" wound (wrapped) about a magnetic induction core to allow amp restriction (minimizing current leakage) while encouraging "**Voltage Potential**" ($V_a \times V_n$) across the water molecule to perform WFC "**Electrical Polarization Process**", as so illustrated in Figure (7-1) **WFC memo** (426) titled **VIC Matrix Circuit**.



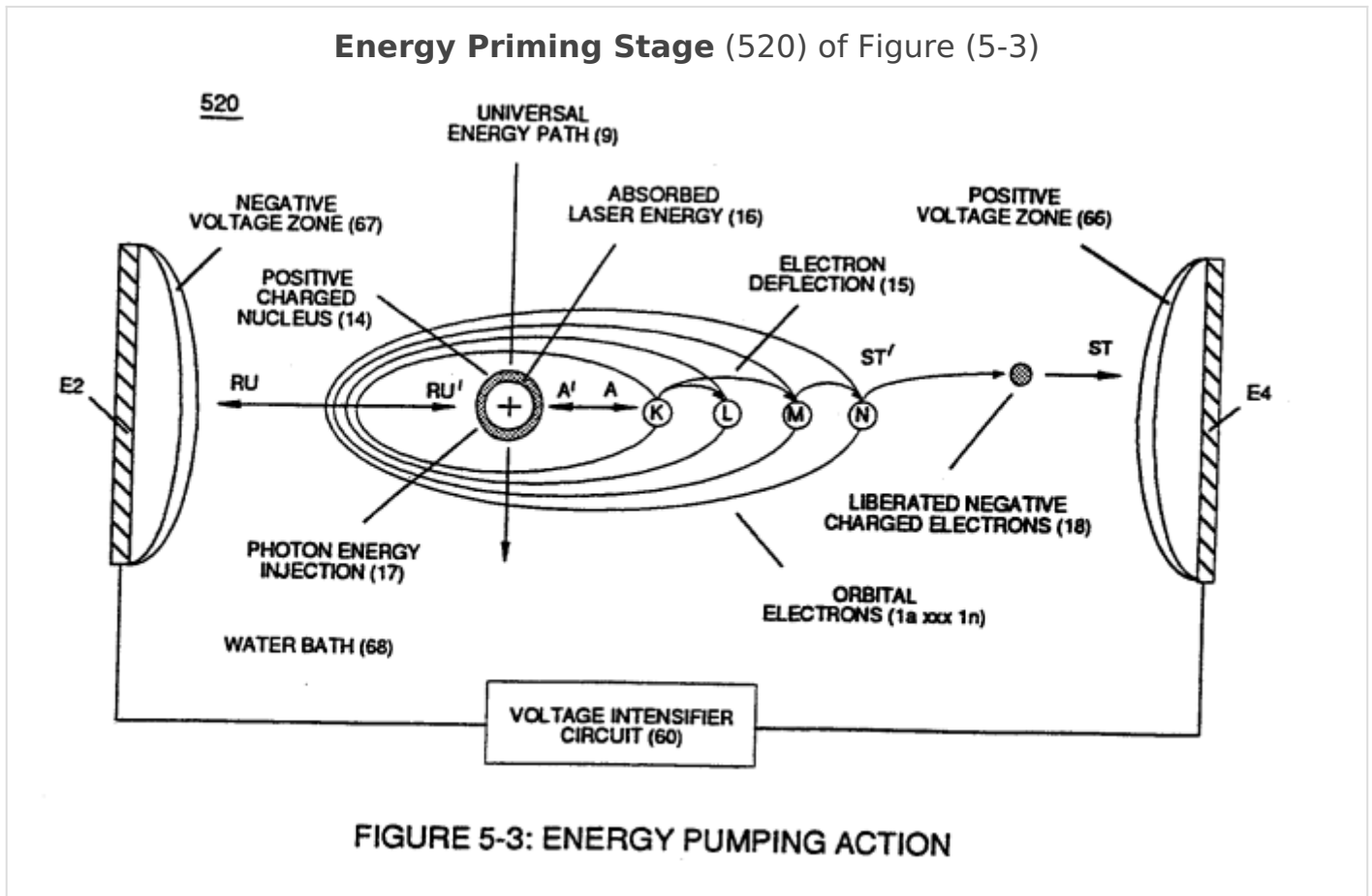
The energized "**Resonant Charging Choke**" (56) of Figure (7-1) as to Figure (10-1) by way of input voltage-pulses (49a xxx 49n) creates an **electromagnetic coupling field** (Rp1) of Figure (7-8) due to its **self-inductance** (640) of Figure 7-3B) crosses over and passes through electrically ground connected **Resonant Charging Choke** (62), as so illustrated in Figure (10-1)



... causing amp flow restriction during each pulsing-cycle since electrons exhibit electromagnetic characteristic

... forming "**Mutual Inductance Fields**" (Rp1/Rp2) once **secondary coil** (62) is electromagnetically energized by **primary coil** (56) and vice versa

... thereby, preventing amp "in-fluxing" (discouraging electron arc over) across **Dielectric Capacitor Gap** (ER)(66/67) while **Electrical Stress** (ST-ST' - RU-RU') of **Opposite Voltage Polarity** (B+/B-) brings on **Energy Priming Stage** (520) of Figure (5-3) which is refer to, herein, as "**Voltage Tickling of State Space**."



The resultant **Amp Inhibiting Circuit** Figure (10-1) as to Figure (10-3 A/B) further allows amp restriction (minimizing current leakage) to be continued even if applied "**Voltage Amplitude**" is increased. The length and diameter size of the copper-wire spiral wrapped coil (56/62) of Figure (10-1) being paired together and electrically energized in conjunction with applied **Voltage Pulse-Frequency** determines how much "**Amp Leakage**" will occur across capacitor **Gap** (Cp) while "**Voltage Pulse-Potential**" (Va xxx Vn/49a xxx 49n) of "**Opposite polarity**" (B+/B-) is/are allowed to be applied across "**Electrical Voltage Plates**" (Voltage-Zones) (66/67).

Amp Inhibiting Circuit Figure (10-1)

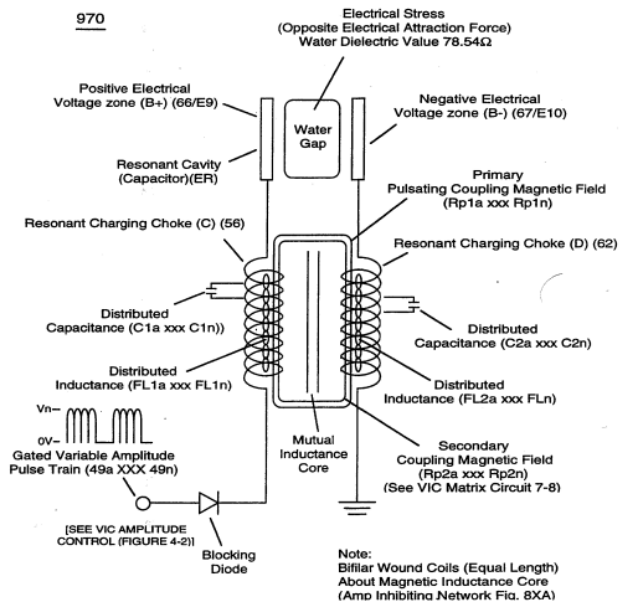
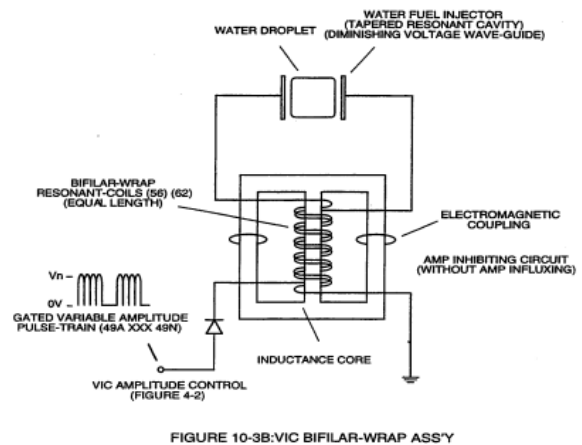
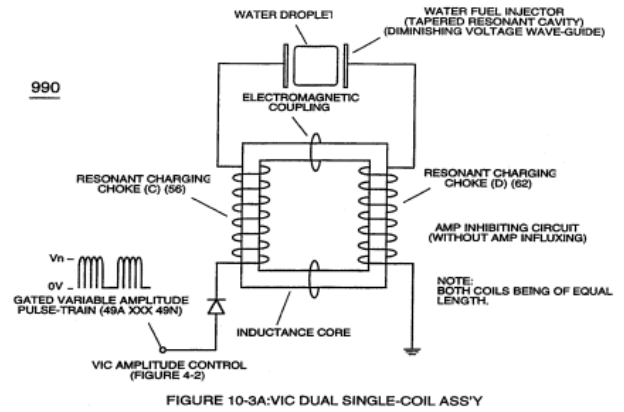


Figure (10-3 A/B)



To reduce amp leakage still further, the copper wire of both **Resonant Charging Chokes** (56/62) can be replaced with a magnetically inductive stainless steel wire (430F/FR) having a resistive value (Ohms) to the flow of electrons while taking on the capacitance and inductance characteristic of a coil wire.

VIC **Bifilar Wrap Coil-Assembly** (10-3B) and VIC **Dual Coil Wrap-Assembly** (10-3A) both utilize either "E" & "I" and "U" Inductance Core configurations to concentrate Mutual Inductance Fields (Rp1/Rp2) in order to optimize **Amp Inhibiting Process** (750) of Figure (7-14).

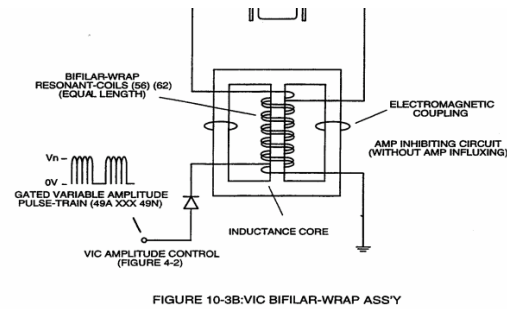


FIGURE 10-3B: VIC BIFILAR-WRAP ASS'Y

FIGURE 10-3: VIC COIL-WRAP CONFIGURATION

"E" "I" core shape (10-3B) is **most preferable**

since amp spike surge is minimize during repetitive pulsing operations.

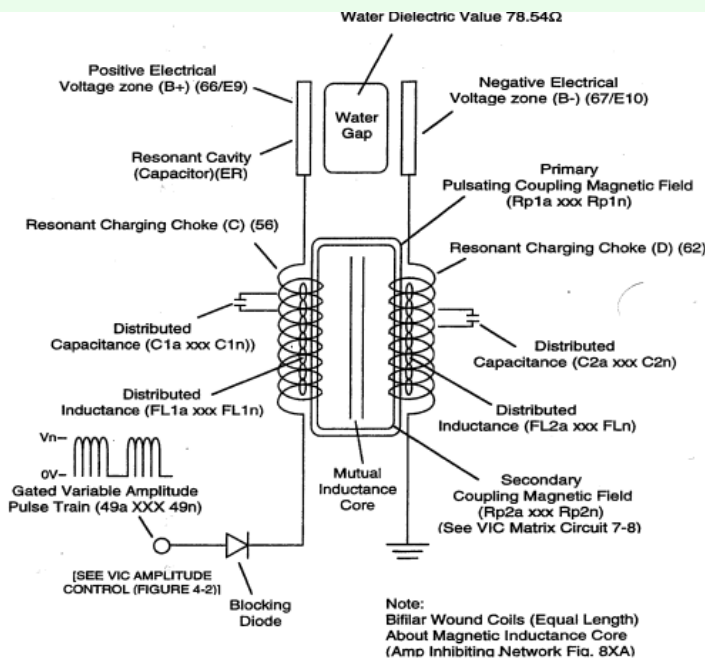


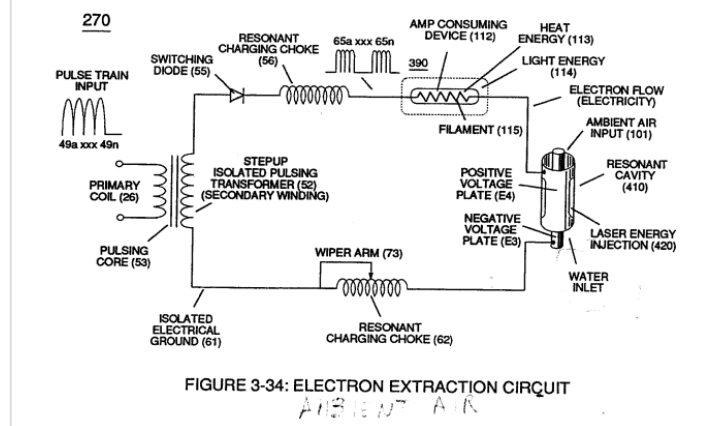
FIGURE 10-1: VOLTAGE INTENSIFIER CIRCUIT

Beyond amp restricting characteristic

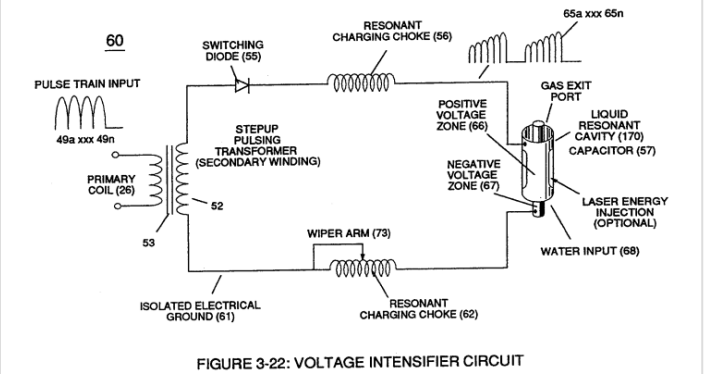
of said **Amp Inhibiting Circuit** (970) of Figure (10-1) as to **Voltage Intensifier Circuit** (60) of Figure (3-22), the spiral-wrapped coils (**Resonant Charging Chokes** 56/62) being paired together, also, causes voltage level enhancement beyond applied voltage input since the "**Distributed Capacitance**" (C1a xxx C1n - C2a xxx C2n) / "**Distributed Inductance**" (FL1a xxx FL1n - FL2a xxx FL2n) of said "bifilar" wrapped coils (Figure 7-3) as to (990) of Figure (10-3) encourages the compounding effect (increasing magnetic field-strength during each pulsing cycle) of electromagnetic field-

strength (Rp1a xxx Rp1n - Rp2a xxx Rp2n) (mutual induction) when applied **Pulse-Voltage** frequency (49a xxx 49n) of Figure (3-34) passes through the positive energized **Resonant Charging Choke** (56).

Figure (3-34)



Voltage Intensifier Circuit (60) of Figure (3-22)



"bifilar" wrapped coils (Figure 7-3)

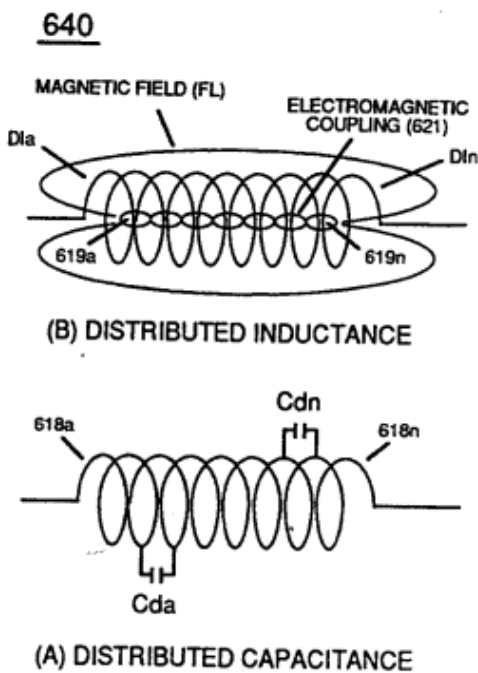


FIGURE 7-3: COIL INTERACTION

(990) of Figure (10-3)

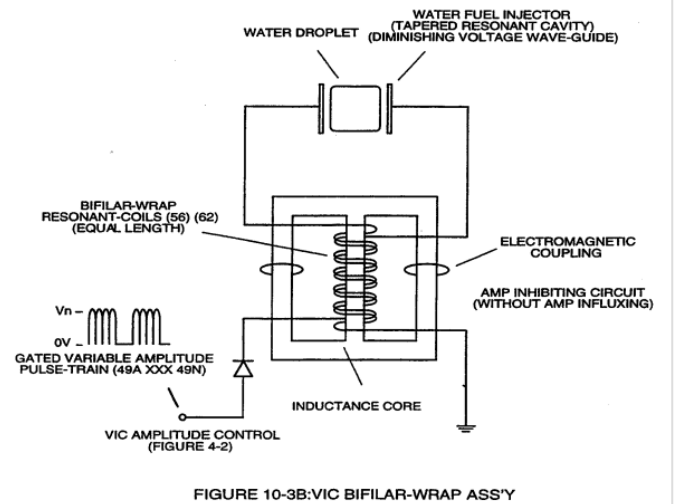


FIGURE 10-3: VIC COIL-WRAP CONFIGURATION

Furthermore, the paired coil-wires opposite voltage potential [**positiveelectrical attraction force** (B+) - **negative electrical attraction force** (B-)] [hereinafter called **Electrical Stress** (SS' - RR') as to (160) of Figure (3-26)] are always **equal** in electrical magnitude/intensity **since the wire-lengths of each coil are the same.**

(160) of Figure (3-26)

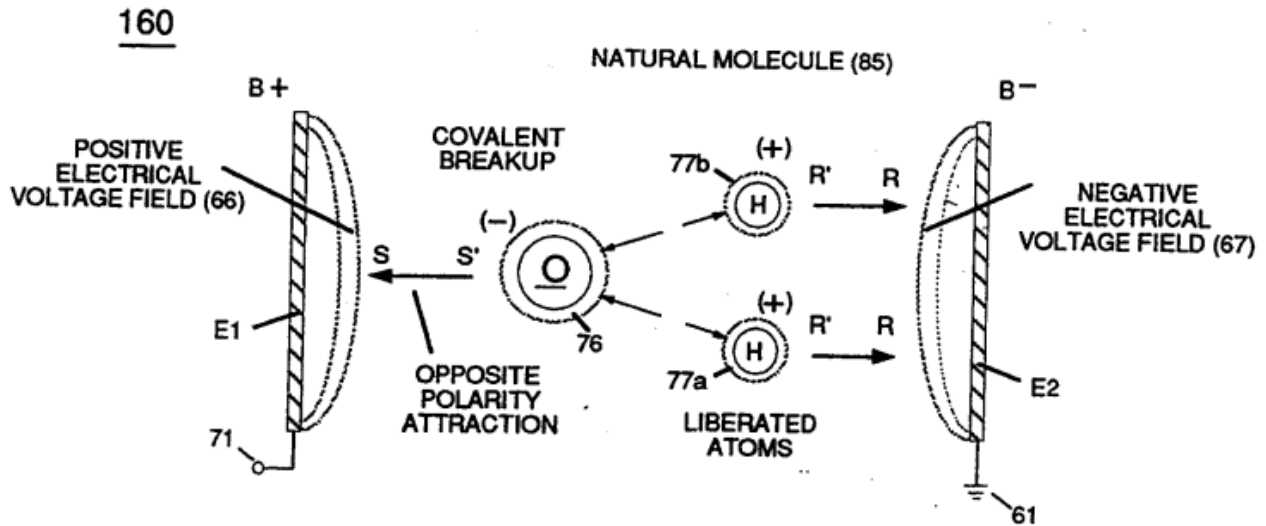


FIGURE 3-26: ELECTRICAL POLARIZATION PROCESS

Pulse-Voltage repetition rate sets up the step-up charging effect Figure (1-3) since the "**Resonant Cavity**" (Cp) functions as a "**Capacitor**" (ER) due to the dielectric value of the liquid (or gases) which becomes an integral part of the VIC Circuit, as so illustrated in (650) of Figure (7-4).

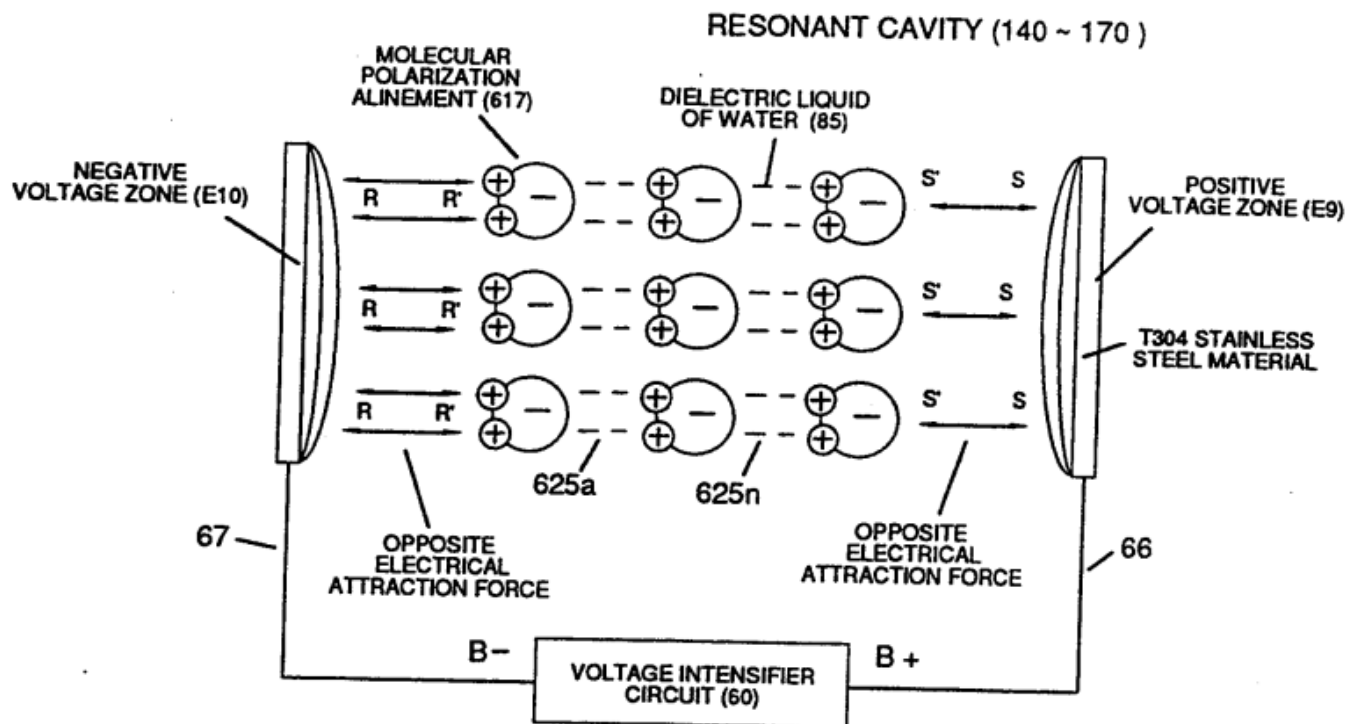


FIGURE 7-4: ELECTRICAL CHARGING EFFECT

The resultant voltage enhancement (**Voltage Amplitude**) can exceed 40 kilovolts to instantly convert water (droplets) into thermal explosive energy (gtnt) on demand, as so illustrated in **Voltage Intensifier Circuit Diagram (970)** of Figure (10-1).

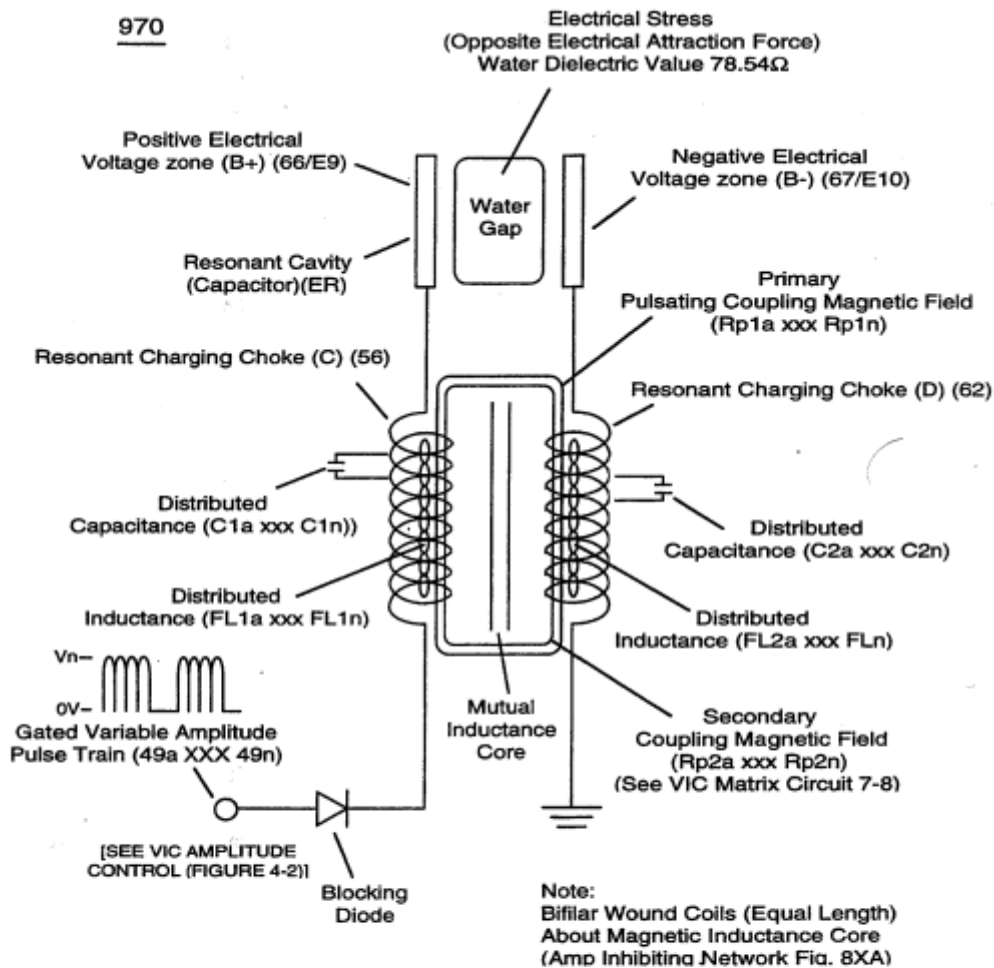


FIGURE 10-1: VOLTAGE INTENSIFIER CIRCUIT

Blocking Diode (52) of Figure (4-9) as to Figure (1-1) allows **unipolar pulse-wave** to go more positive on each pulse-cycle since the **Blocking Diode** (52) prevents the **Resonant Cavity** (Cp) from discharging during pulse off-time, as so illustrated in Figure (1-4) as to (60) of Figure (3-22)

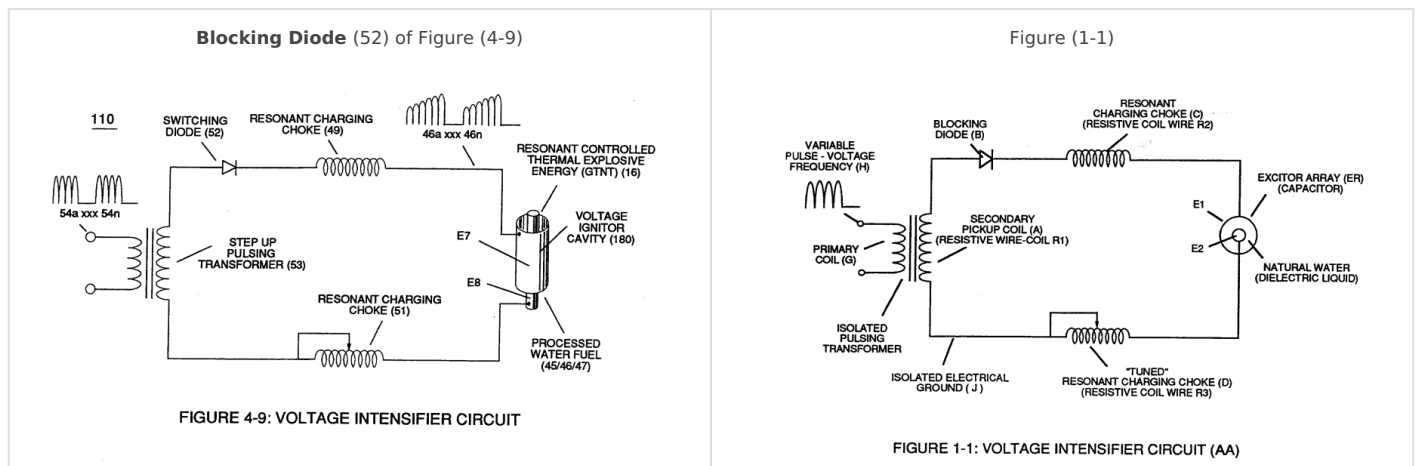


Figure (1-4)

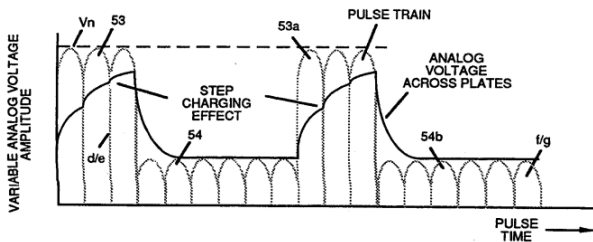


FIGURE 1-4: APPLIED VOLTAGE TO RESONANT CAVITY

(60) of Figure (3-22)

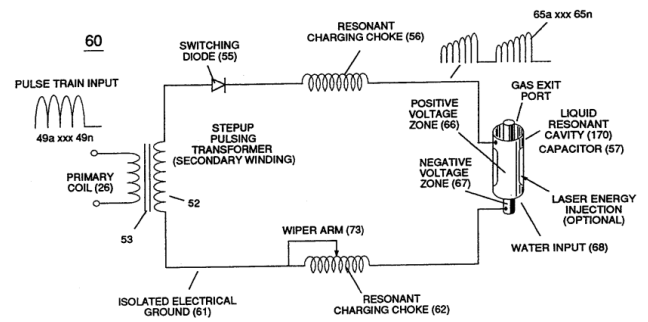


FIGURE 3-22: VOLTAGE INTENSIFIER CIRCUIT

... allowing the developed "**Electrical Stress**" ($RU/RU' - ST/ST'$) of Figure (5-1/5-2) across **Capacitor Gap** (C_p) to go to the farthest point beyond the "**State of Equilibrium**"

Figure (5-1)

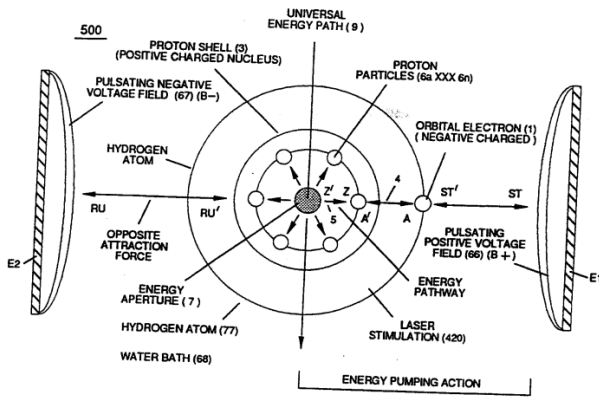


FIGURE 5-1: HYDROGEN ENERGY BALANCE

Figure (5-2)

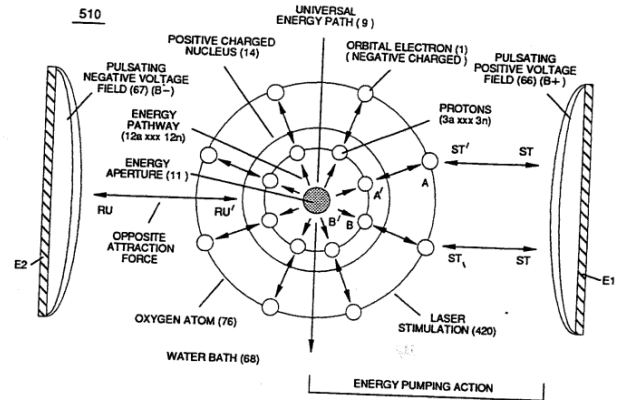


FIGURE 5-2: OXYGEN ENERGY BALANCE

... see Atomic Energy Balance of Water (WFC memo 424), once again.

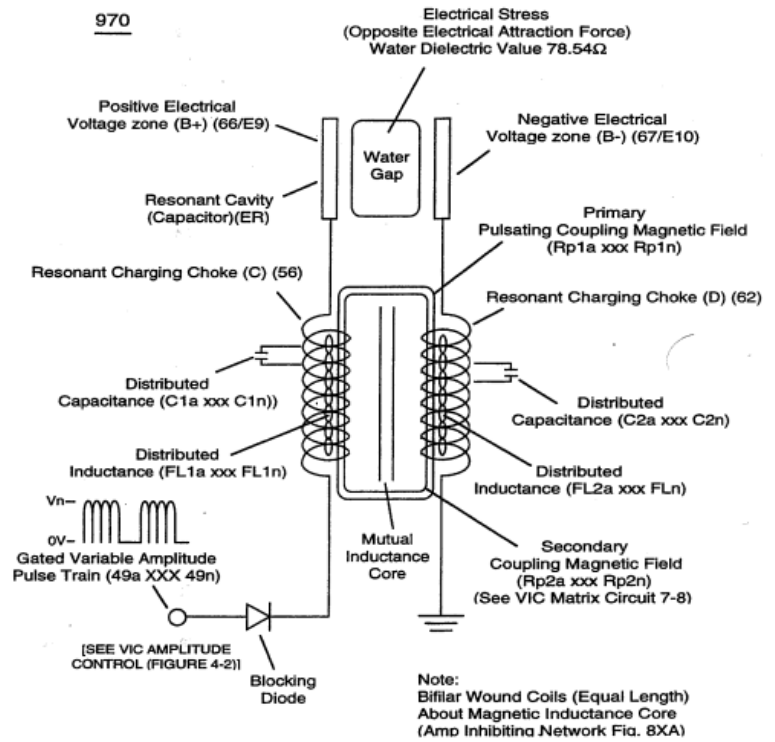


FIGURE 10-1: VOLTAGE INTENSIFIER CIRCUIT

The programmable pulse-frequency (49a xxx 49n) of Figure (10-1) input is simply adjusted to tune-in to the dielectric property of the **Water Molecule**.

The resultant **Dynamic Electrical Charging Effect** (612) of Figure (8-1) acts as a progressive energy enhancer (**Energy Priming Stage**) (500) of Figure (5-1)

Dynamic Electrical Charging Effect
(612) of Figure (8-1)

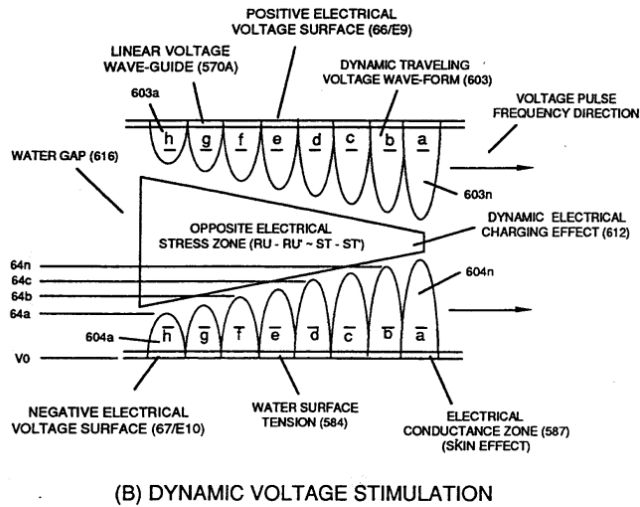


FIGURE 8-1: ELECTRICAL CHARGING STAGE

Energy Priming Stage (500) of Figure (5-1)

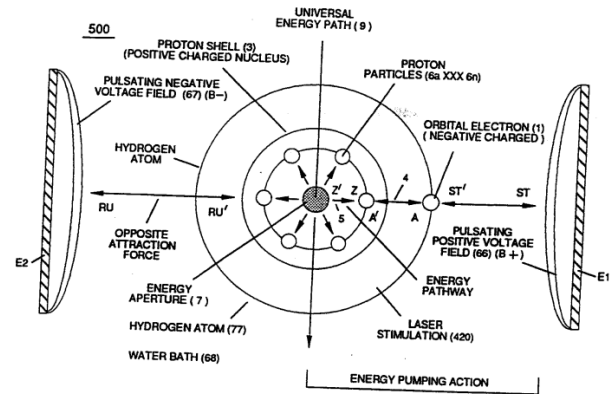


FIGURE 5-1: HYDROGEN ENERGY BALANCE

when **Static State Space** (790) of (8-3) is configured to **Dynamic State Space** (800) of Figure (8-4), as so illustrated in [WFC memo \(427\)](#) titled "**Voltage Wave-Guide**"

Static State Space (790) of (8-3)

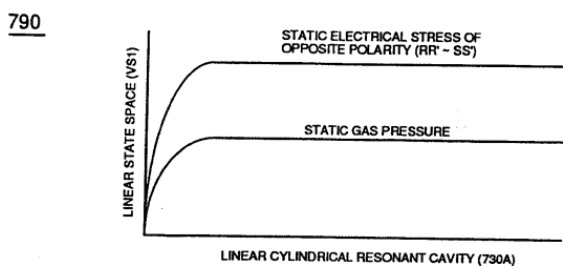


FIGURE 8-3: STATIC VARIABLES

Dynamic State Space (800) of Figure (8-4)

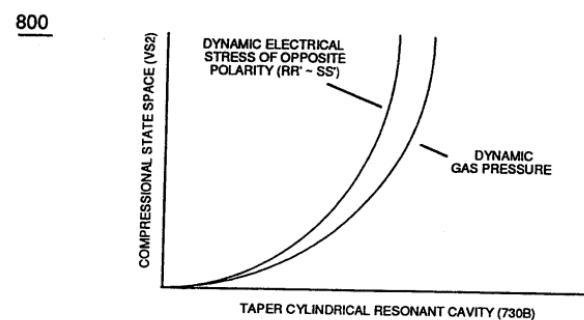


FIGURE 8-4: DYNAMIC VARIABLES

... whereby, the **Voltage Wave-Guides** forms **Water Gap** (Cp).