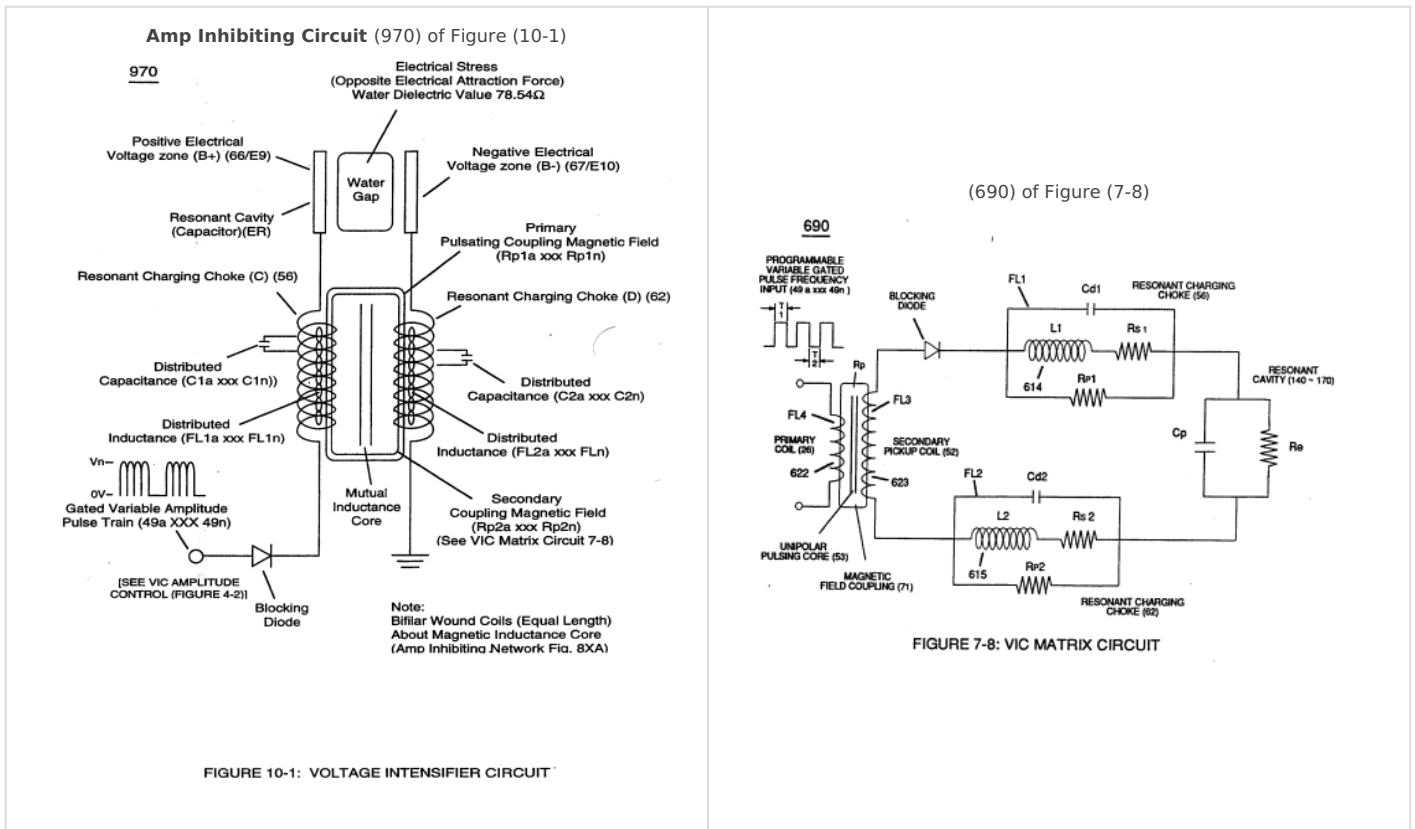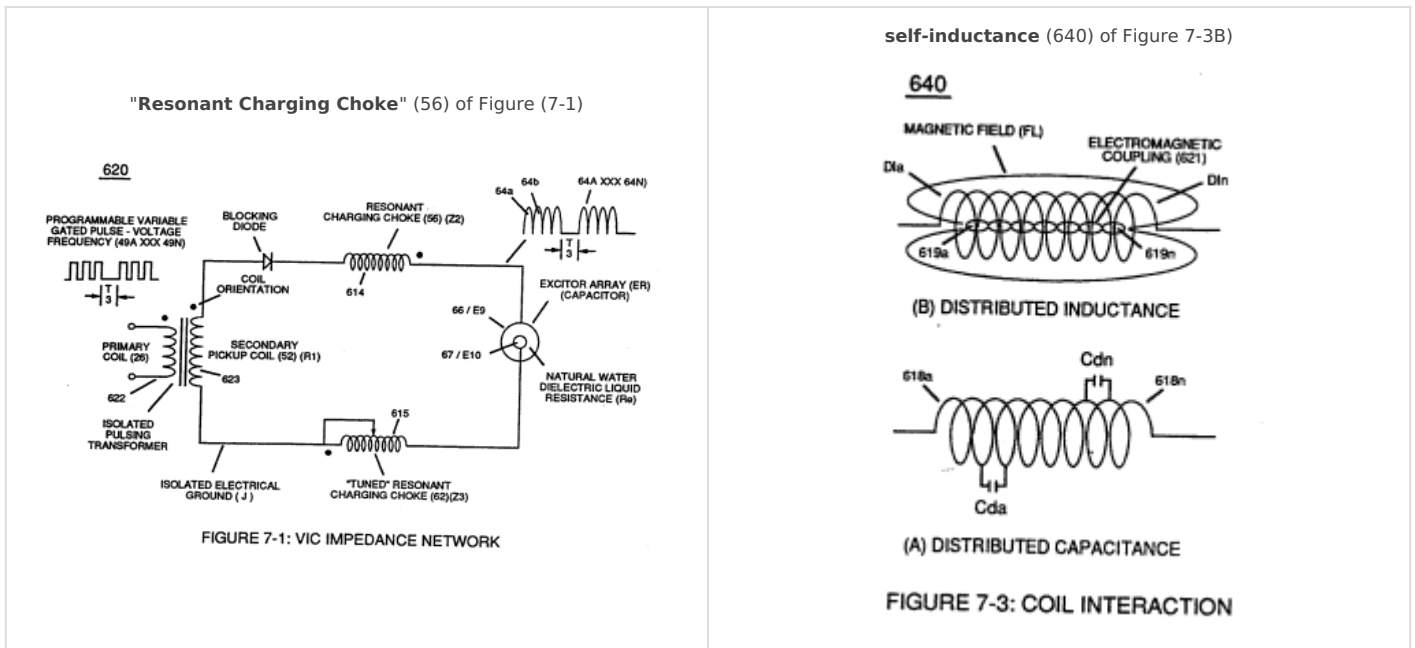# Propagating Electrical Stress

As in reference to **WFC Patent Validation Report** dated January 14, 1983 as per **WFC Test-Results** "Mode of Operability" of using "**Voltage Potential**" to "**Dissociates the Water Molecule**" by way of the "**Electrical Polarization Process**" (160) of Figure (3-26) as so specified under U.S. Patent Law (35 USC 101) demonstrate operability, the applied **Pulse-Voltage Frequency** is adjusted to tune-in to the dielectric properties of water by the use of WFC "**Amp Inhibiting Circuit**" (970) of Figure (10-1), as further illustrated in **WFC Tech-Brief** titled "**The Birth of New Technology**"

> ... U.S. Patent Memos 420 - 428, including "Table of Tabulation" (Appendix A) as to "Glossary of Application Notes" (Appendix B).

The **Amp Inhibiting Circuit** (970) of Figure (10-1) as to (690) of Figure (7-8) is composed of two copper wires "**Bifilar**" wound (wrapped) about a magnetic induction core to allow amp restriction (minimizing current leakage) while encouraging "**Voltage Potential**"(Va xxx Vn) across the water molecule to perform WFC "**Electrical Polarization Process**", as so illustrated in Figure (7-1) WFC memo (426) titled **VIC Matrix Circuit**.

Amp Inhibiting Circuit (970) of Figure (10-1)

970

Electrical Stress
(Opposite Electrical Attraction Force)
Water Dielectric Value 78.54Ω

Positive Electrical
Voltage zone (B+) (66/E9)

Negative Electrical
Voltage zone (B-) (67/E10)

Water Gap

Resonant Cavity
(Capacitor)(ER)

Primary
Pulsating Coupling Magnetic Field
(Rp1a xxx Rp1n)

Resonant Charging Choke (C) (56)

Resonant Charging Choke (D) (62)

Distributed
Capacitance (C1a xxx C1n))

Distributed
Capacitance (C2a xxx C2n)

Distributed
Inductance (FL1a xxx FL1n)

Distributed
Inductance (FL2a xxx FLn)

Vn~
0V~

Gated Variable Amplitude
Pulse Train (49a XXX 49n)

Mutual
Inductance
Core

Secondary
Coupling Magnetic Field
(Rp2a xxx Rp2n)
(See VIC Matrix Circuit 7-8)

[SEE VIC AMPLITUDE
CONTROL (FIGURE 4-2)]

Blocking
Diode

Note:
Bifilar Wound Coils (Equal Length)
About Magnetic Inductance Core
(Amp Inhibiting Network Fig. 8XA)

FIGURE 10-1: VOLTAGE INTENSIFIER CIRCUIT

---

(690) of Figure (7-8)

690

PROGRAMMABLE
VARIABLE GATED
PULSE FREQUENCY
INPUT (49 a xxx 49n)

BLOCKING
DIODE

FL1
Cd1
RESONANT CHARGING
CHOKE (56)

L1
Rs 1

Rp
614
Rp1

FL3

FL4
PRIMARY
COIL (26)
622

SECONDARY
PICKUP COIL (52)
623

RESONANT
CAVITY (140 ~ 170)

Cp
Re

FL2
Cd2

L2
Rs 2

UNIPOLAR
PULSING CORE (53)

615
Rp2

MAGNETIC
FIELD COUPLING (71)

RESONANT CHARGING
CHOKE (62)

FIGURE 7-8: VIC MATRIX CIRCUIT

The energized "**Resonant Charging Choke**" (56) of Figure (7-1) as to Figure (10-1) by way of input voltage-pulses (49a xxx 49n) creates an **electromagnetic coupling field** (Rp1) of Figure (7-8) due to its **self-inductance** (640) of Figure 7-3B) crosses over and passes through electrically ground connected **Resonant Charging Choke** (62), as so illustrated in Figure (10-1)

"**Resonant Charging Choke**" (56) of Figure (7-1)

620

PROGRAMMABLE VARIABLE
GATED PULSE - VOLTAGE
FREQUENCY (49A XXX 49N)

BLOCKING
DIODE

RESONANT
CHARGING CHOKE (56) (Z2)

64a
64b
64A XXX 64N

COIL
ORIENTATION
614

EXCITOR ARRAY (ER)
(CAPACITOR)

66 / E9

PRIMARY
COIL (26)

SECONDARY
PICKUP COIL (52) (R1)
623

67 / E10

NATURAL WATER
DIELECTRIC LIQUID
RESISTANCE (Re)

622

ISOLATED
PULSING
TRANSFORMER

615

ISOLATED ELECTRICAL
GROUND (J)

"TUNED" RESONANT
CHARGING CHOKE (62)(Z3)

FIGURE 7-1: VIC IMPEDANCE NETWORK

---

self-inductance (640) of Figure 7-3B)

640

MAGNETIC FIELD (FL)

ELECTROMAGNETIC
COUPLING (621)

Dia
Din

619a
619n

(B) DISTRIBUTED INDUCTANCE

Cdn

618a
618n

Cda

(A) DISTRIBUTED CAPACITANCE

FIGURE 7-3: COIL INTERACTION

... causing amp flow restriction during each pulsing-cycle since electrons exhibit electromagnetic characteristic

... forming "**Mutual Inductance Fields**" (Rp1/Rp2) once **secondary coil** (62) is electromagnetically energized by **primary coil** (56) and vice versa

> ... thereby, preventing amp "in-fluxing" (discouraging electron arc over) across **Dielectric Capacitor Gap** (ER)(66/67) while **Electrical Stress** (ST-ST' - RU-RU') of **Opposite Voltage Polarity** (B+/B-) brings on **Energy Priming Stage** (520) of Figure (5-3) which is refer to, herein, as "**Voltage Tickling of State Space**."

Energy Priming Stage (520) of Figure (5-3)

FIGURE 5-3: ENERGY PUMPING ACTION
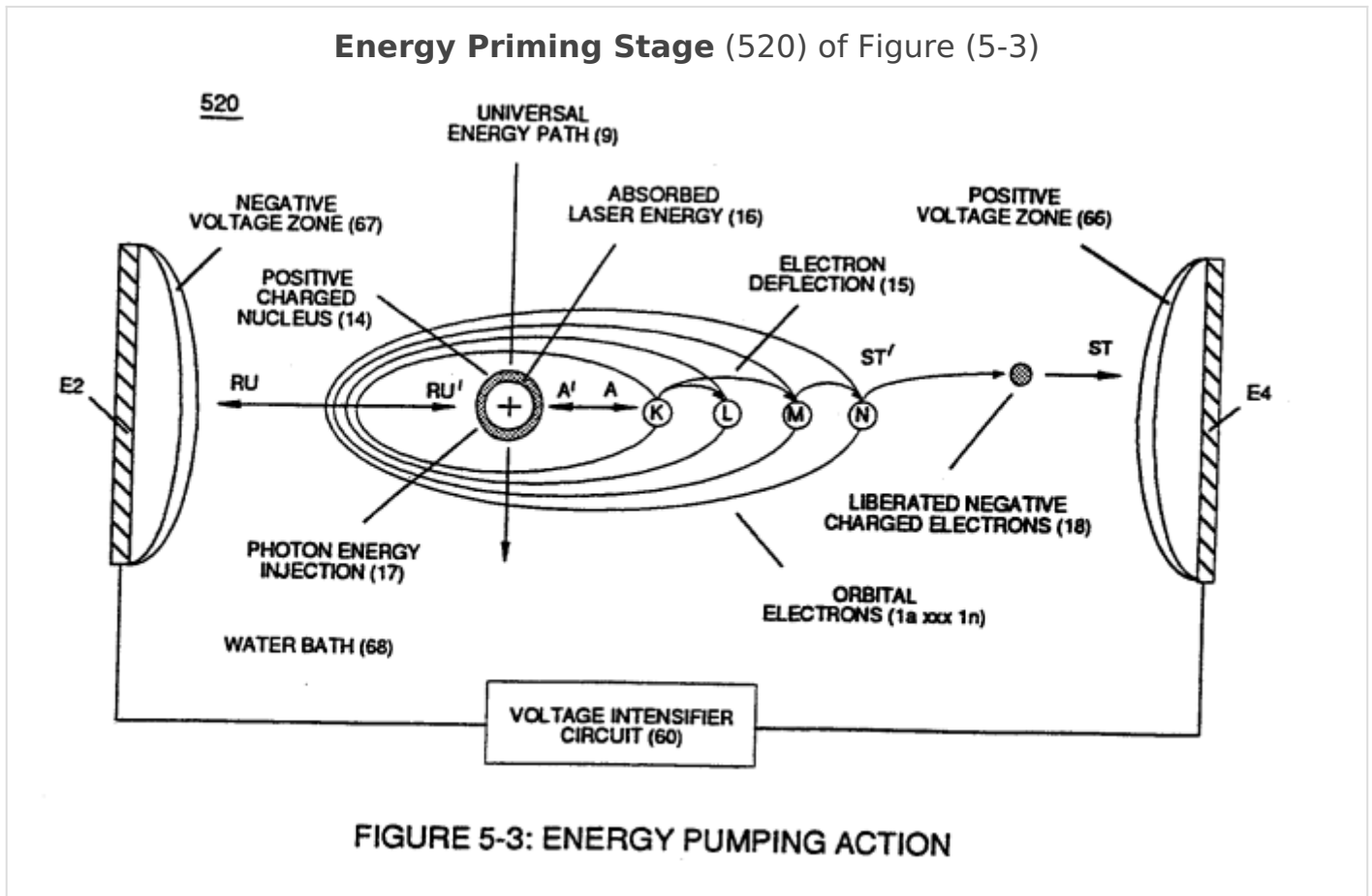
The resultant **Amp Inhibiting Circuit** Figure (10-1) as to Figure (10-3 A/B) further allows amp restriction (minimizing current leakage) to be continued even if applied "**Voltage Amplitude**" is increased. The length and diameter size of the copper-wire spiral wrapped coil (56/62) of Figure (10-1) being paired together and electrically energized in conjunction with applied **Voltage Pulse-Frequency** determines how much "**Amp Leakage**" will occur across capacitor **Gap** (Cp) while "**Voltage Pulse-Potential**" (Va xxx Vn/49a xxx 49n) of "**Opposite polarity**" (B+/B-) is/are allowed to be applied across "**Electrical Voltage Plates**" (Voltage-Zones) (66/67).
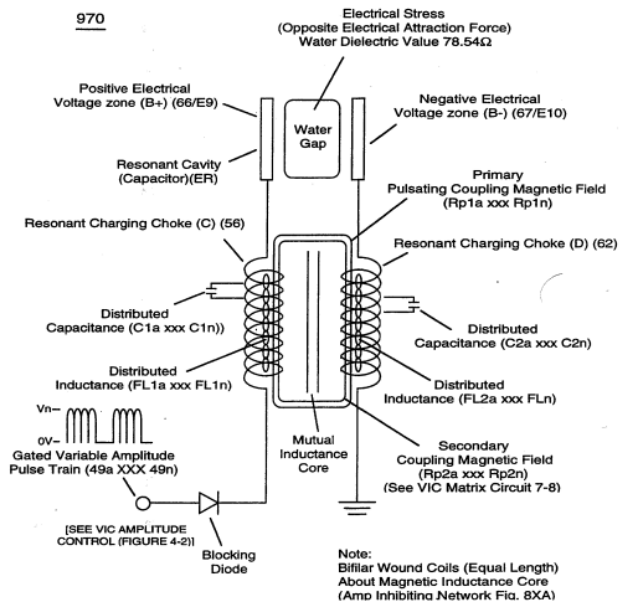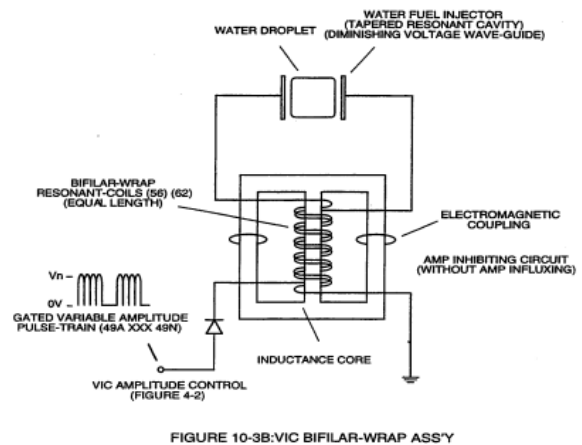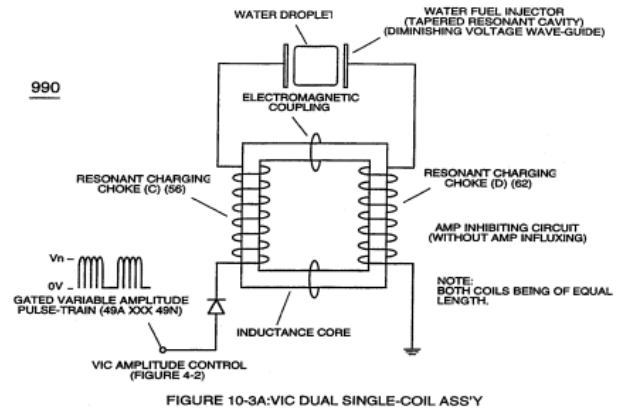
Amp Inhibiting Circuit Figure (10-1)

970

Electrical Stress
(Opposite Electrical Attraction Force)
Water Dielectric Value 78.54Ω

Positive Electrical
Voltage zone (B+) (66/E9)

Negative Electrical
Voltage zone (B-) (67/E10)

Water Gap

Resonant Cavity
(Capacitor)(ER)

Primary
Pulsating Coupling Magnetic Field
(Rp1a xxx Rp1n)

Resonant Charging Choke (C) (56)

Resonant Charging Choke (D) (62)

Distributed
Capacitance (C1a xxx C1n))

Distributed
Capacitance (C2a xxx C2n)

Distributed
Inductance (FL1a xxx FL1n)

Distributed
Inductance (FL2a xxx FLn)

Vn−
0V−
Gated Variable Amplitude
Pulse Train (49a XXX 49n)

Mutual
Inductance
Core

Secondary
Coupling Magnetic Field
(Rp2a xxx Rp2n)
(See VIC Matrix Circuit 7-8)

[SEE VIC AMPLITUDE
CONTROL (FIGURE 4-2)]

Blocking
Diode

Note:
Bifilar Wound Coils (Equal Length)
About Magnetic Inductance Core
(Amp Inhibiting Network Fig. 8XA)

FIGURE 10-1: VOLTAGE INTENSIFIER CIRCUIT

Figure (10-3 A/B)

990

WATER DROPLET

WATER FUEL INJECTOR
(TAPERED RESONANT CAVITY)
(DIMINISHING VOLTAGE WAVE-GUIDE)

ELECTROMAGNETIC
COUPLING

RESONANT CHARGING
CHOKE (C) (56)

RESONANT CHARGING
CHOKE (D) (62)

AMP INHIBITING CIRCUIT
(WITHOUT AMP INFLUXING)

Vn−
0V−
GATED VARIABLE AMPLITUDE
PULSE-TRAIN (49A XXX 49N)

NOTE:
BOTH COILS BEING OF EQUAL
LENGTH.

INDUCTANCE CORE

VIC AMPLITUDE CONTROL
(FIGURE 4-2)

FIGURE 10-3A:VIC DUAL SINGLE-COIL ASS'Y

WATER DROPLET

WATER FUEL INJECTOR
(TAPERED RESONANT CAVITY)
(DIMINISHING VOLTAGE WAVE-GUIDE)

BIFILAR-WRAP
RESONANT-COILS (56) (62)
(EQUAL LENGTH)

ELECTROMAGNETIC
COUPLING

AMP INHIBITING CIRCUIT
(WITHOUT AMP INFLUXING)

Vn−
0V−
GATED VARIABLE AMPLITUDE
PULSE-TRAIN (49A XXX 49N)

INDUCTANCE CORE

VIC AMPLITUDE CONTROL
(FIGURE 4-2)

FIGURE 10-3B:VIC BIFILAR-WRAP ASS'Y

To reduce amp leakage still further, the copper wire of both **Resonant Charging Chokes** (56/62) can be replaced with a magnetically inductive stainless steel wire (430F/FR) having a resistive value (Ohms) to the flow of electrons while taking on the capacitance and inductance characteristic of a coil wire.

VIC **Bifilar Wrap Coil-Assembly** (10-3B) and VIC **Dual Coil Wrap-Assembly** (10-3A) both utilize either "E" & "I" and "U" Inductance Core configurations to concentrate Mutual Inductance Fields (Rpl/Rp2) in order to optimize **Amp Inhibiting Process** (750) of Figure (7-14).
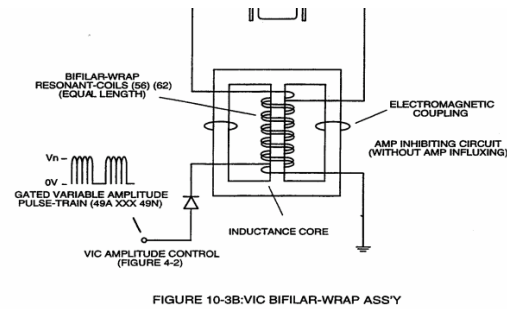
FIGURE 10-3B:VIC BIFILAR-WRAP ASS'Y

FIGURE 10-3: VIC COIL-WRAP CONFIGURATION

"E" "I" core shape (10-3B) is **most preferable** since amp spike surge is minimize during repetitive pulsing operations.
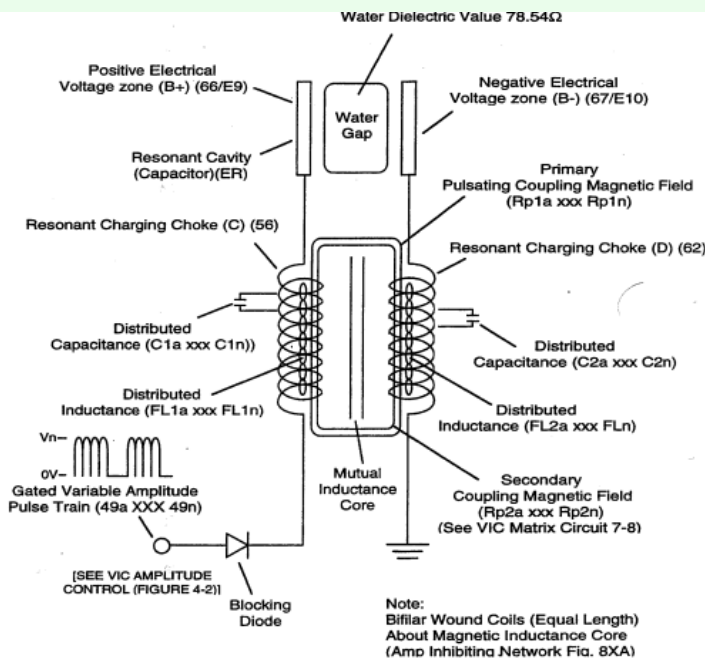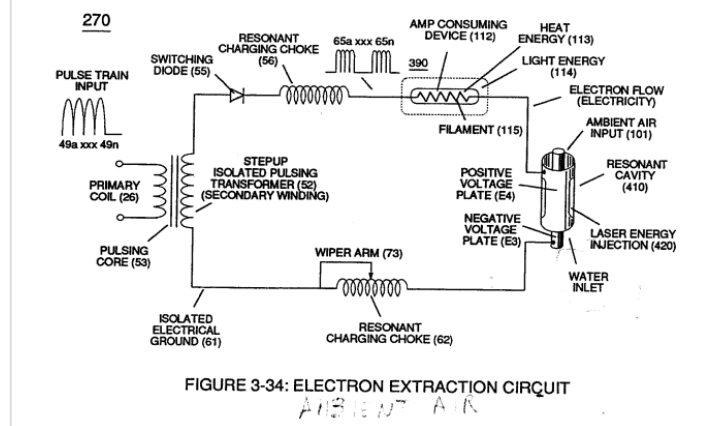

FIGURE 10-1: VOLTAGE INTENSIFIER CIRCUIT

Beyond amp restricting characteristic of said **Amp Inhibiting Circuit** (970) of Figure (10-1) as to **Voltage Intensifier Circuit** (60) of Figure (3-22), the spiral-wrapped coils (**Resonant Charging Chokes** 56/62) being paired together, also, causes voltage level enhancement beyond applied voltage input since the "**Distributed Capacitance**" (C1a xxx C1n - C2a xxx C2n) / "**Distributed Inductance**" (FL1a xxx FL1n - FL2a xxx FL2n) of said "bifilar" wrapped coils (Figure 7-3) as to (990) of Figure (10-3) encourages the compounding effect (increasing magnetic field-strength during each pulsing cycle) of electromagnetic field-

strength (Rp1a xxx Rp1n - Rp2a xxx Rp2n) (mutual induction) when applied **Pulse-Voltage** frequency (49a xxx 49n) of Figure (3-34) passes through the positive energized **Resonant Charging Choke** (56).

Figure (3-34)

FIGURE 3-34: ELECTRON EXTRACTION CIRCUIT

Voltage Intensifier Circuit (60) of Figure (3-22)

FIGURE 3-22: VOLTAGE INTENSIFIER CIRCUIT

"bifilar" wrapped coils (Figure 7-3)

(B) DISTRIBUTED INDUCTANCE

(A) DISTRIBUTED CAPACITANCE
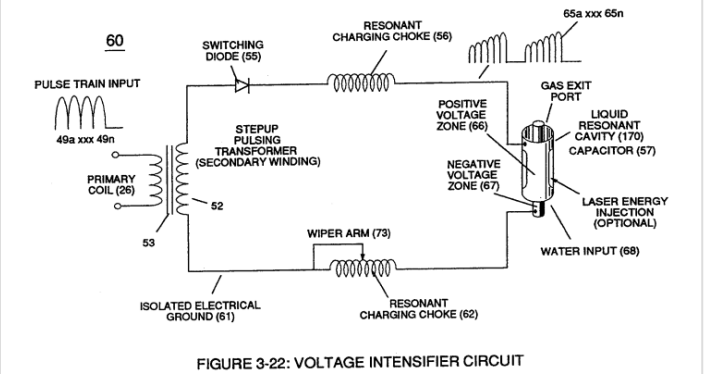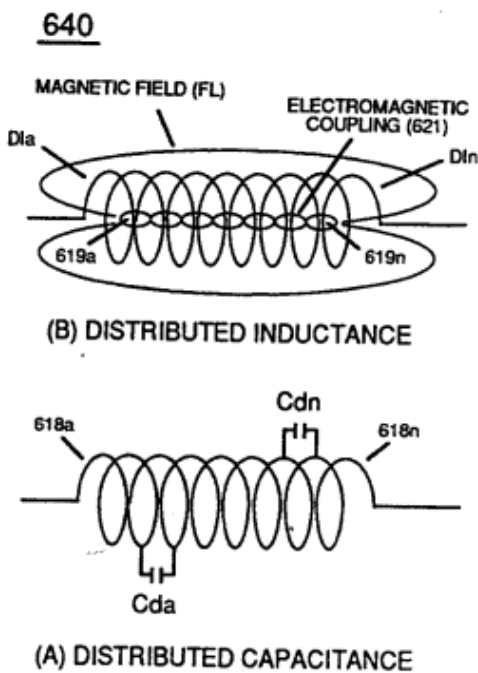
FIGURE 7-3: COIL INTERACTION

(990) of Figure (10-3)

FIGURE 10-3B:VIC BIFILAR-WRAP ASS'Y
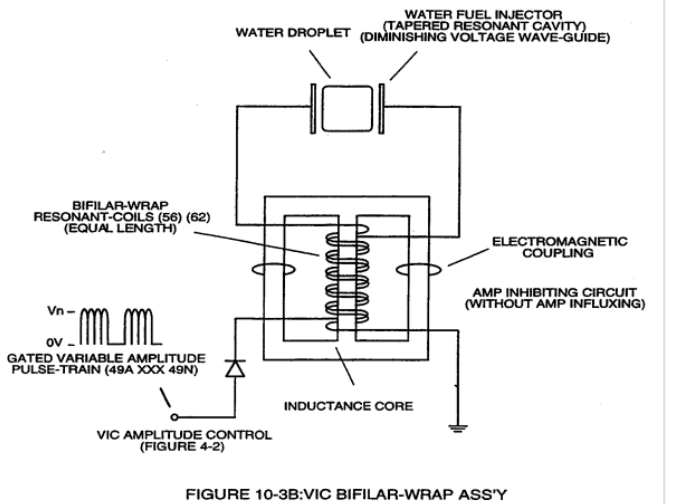
FIGURE 10-3: VIC COIL-WRAP CONFIGURATION

Furthermore, the paired coil-wires opposite voltage potential [**positiveelectrical attraction force** (B+) - **negative electrical attraction force** (B-)] [hereinafter called **Electrical Stress** (SS' - RR') as to (160) of Figure (3-26)] are always **equal** in electrical magnitude/intensity **since the wire-lengths of each coil are the same**.
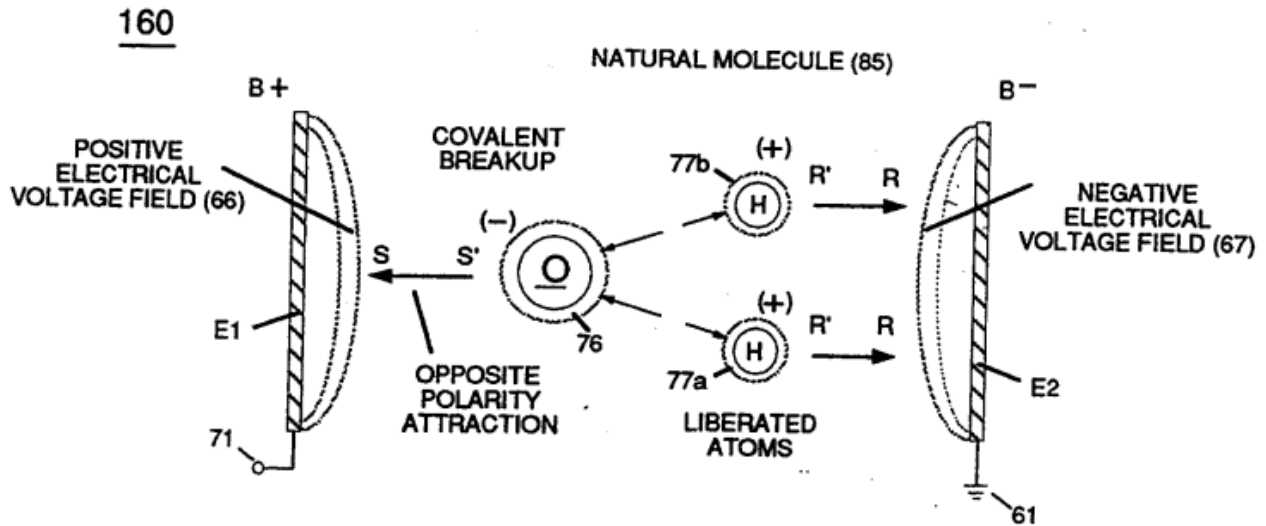
(160) of Figure (3-26)

FIGURE 3-26: ELECTRICAL POLARIZATION PROCESS

Pulse-Voltage repetition rate sets up the step-up charging effect Figure (1-3) since the "**Resonant Cavity**" (Cp) functions as a "**Capacitor**" (ER) due to the dielectric value of the liquid (or gases) which becomes an integral part of the **VIC Circuit**, as so illustrated in (650) of Figure (7-4).

650

RESONANT CAVITY (140 ~ 170)

MOLECULAR
POLARIZATION
ALINEMENT (617)

DIELECTRIC LIQUID
OF WATER (85)

NEGATIVE
VOLTAGE ZONE (E10)

POSITIVE
VOLTAGE ZONE (E9)

T304 STAINLESS
STEEL MATERIAL

625a   625n

67

OPPOSITE
ELECTRICAL
ATTRACTION FORCE

OPPOSITE
ELECTRICAL
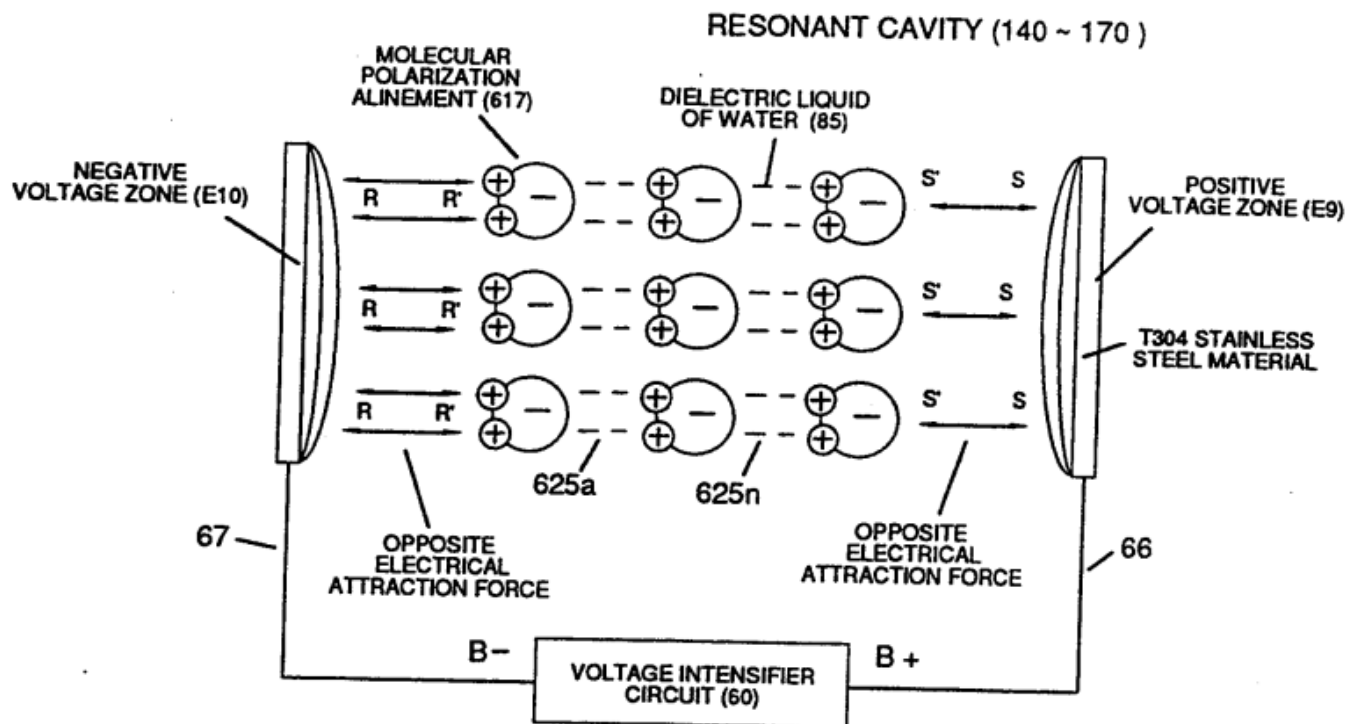ATTRACTION FORCE

66

B−

VOLTAGE INTENSIFIER
CIRCUIT (60)

B +

FIGURE 7-4: ELECTRICAL CHARGING EFFECT

The resultant voltage enhancement (**Voltage Amplitude**) can _exceed 40 kilovolts_ to instantly convert water (droplets) into thermal explosive energy (gtnt) on demand, as so illustrated in **Voltage Intensifier Circuit Diagram** (970) of Figure (10-1).
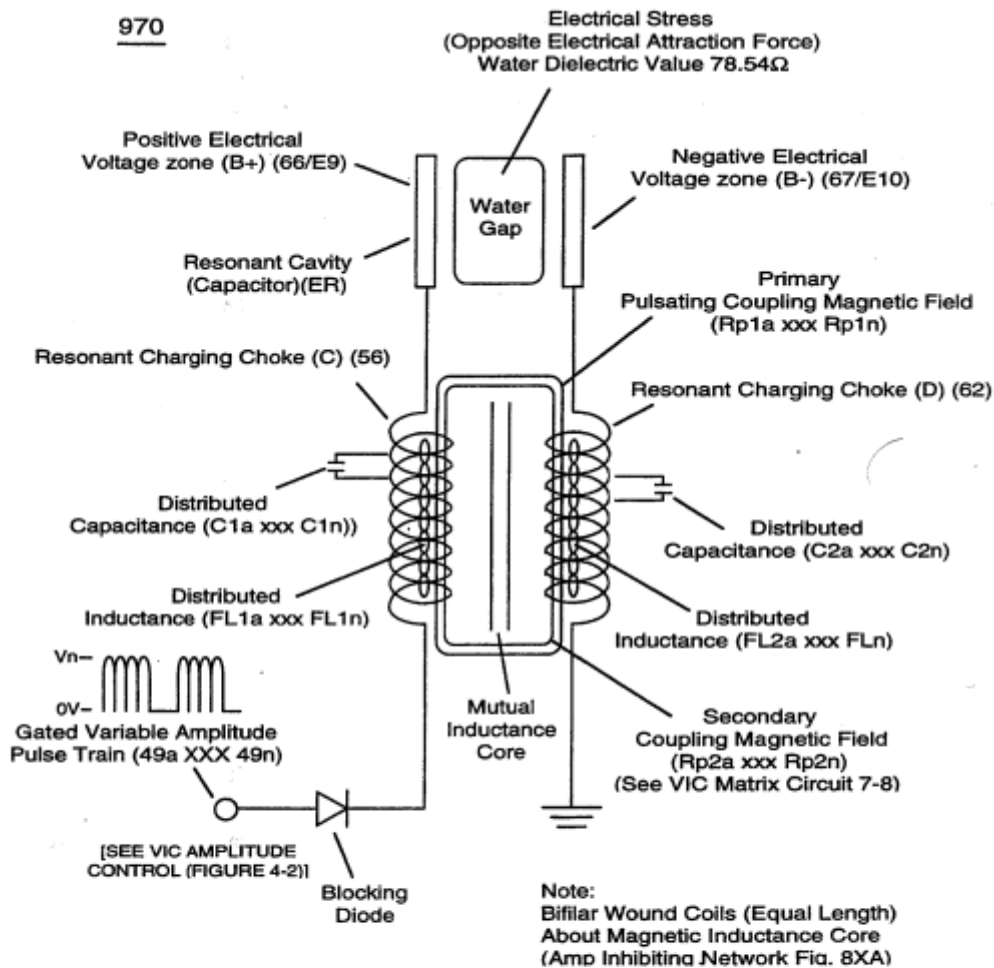
970

FIGURE 10-1: VOLTAGE INTENSIFIER CIRCUIT

Blocking Diode (52) of Figure (4-9) as to Figure (1-1) allows **unipolar pulse-wave** to go <u>more positive</u> on each pulse-cycle since the **Blocking Diode** (52) prevents the **Resonant Cavity** (Cp) from discharging during pulse off-time, as so illustrated in Figure (1-4) as to (60) of Figure (3-22)
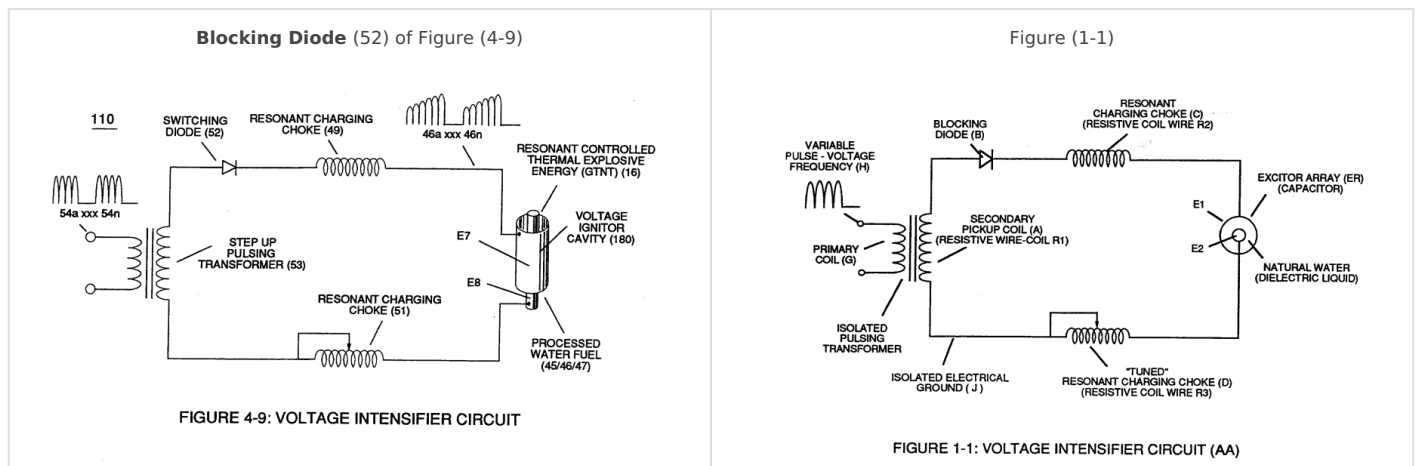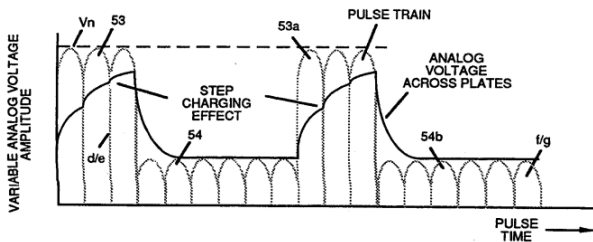

FIGURE 4-9: VOLTAGE INTENSIFIER CIRCUIT

FIGURE 1-1: VOLTAGE INTENSIFIER CIRCUIT (AA)

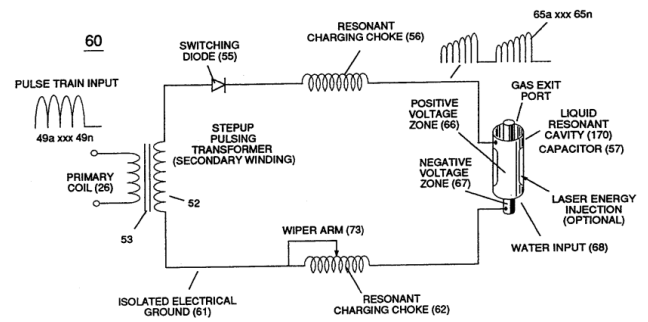Figure (1-4)

FIGURE 1-4: APPLIED VOLTAGE TO RESONANT CAVITY

FIGURE 3-22: VOLTAGE INTENSIFIER CIRCUIT

... allowing the developed "**Electrical Stress**" (RU/RU' - ST/ST') of Figure (5-1/5-2) across **Capacitor Gap** (Cp) to go to the farthest point beyond the "**State of Equilibrium**"
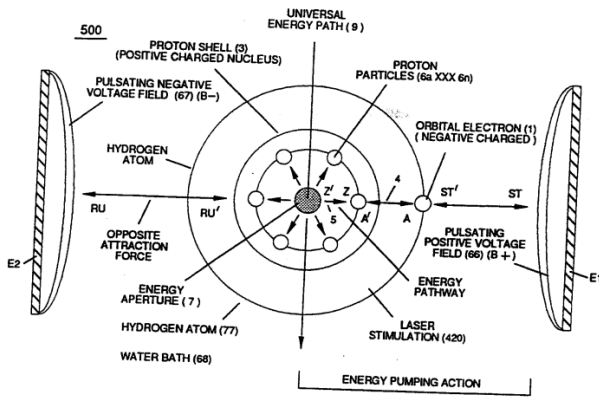
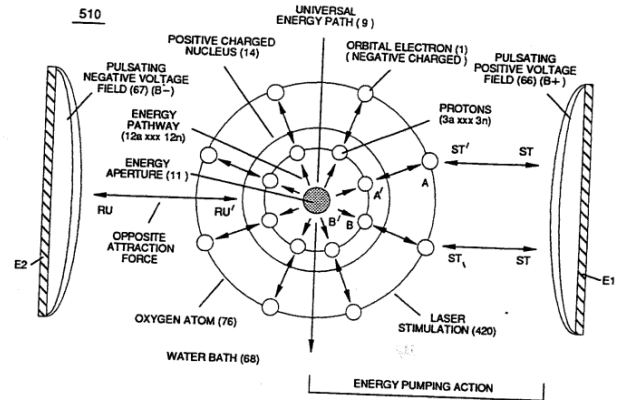Figure (5-1)

FIGURE 5-1: HYDROGEN ENERGY BALANCE

Figure (5-2)

FIGURE 5-2: OXYGEN ENERGY BALANCE

... see Atomic Energy Balance of Water (WFC memo 424), once again.

970

Electrical Stress
(Opposite Electrical Attraction Force)
Water Dielectric Value 78.54Ω

Positive Electrical
Voltage zone (B+) (66/E9)

Water
Gap

Negative Electrical
Voltage zone (B-) (67/E10)

Resonant Cavity
(Capacitor)(ER)

Primary
Pulsating Coupling Magnetic Field
(Rp1a xxx Rp1n)

Resonant Charging Choke (C) (56)

Resonant Charging Choke (D) (62)

Distributed
Capacitance (C1a xxx C1n))

Distributed
Capacitance (C2a xxx C2n)

Distributed
Inductance (FL1a xxx FL1n)

Distributed
Inductance (FL2a xxx FLn)

Vn–

0V–

Gated Variable Amplitude
Pulse Train (49a XXX 49n)

Mutual
Inductance
Core

Secondary
Coupling Magnetic Field
(Rp2a xxx Rp2n)
(See VIC Matrix Circuit 7-8)

[SEE VIC AMPLITUDE
CONTROL (FIGURE 4-2)]

Blocking
Diode

Note:
Biflar Wound Coils (Equal Length)
About Magnetic Inductance Core
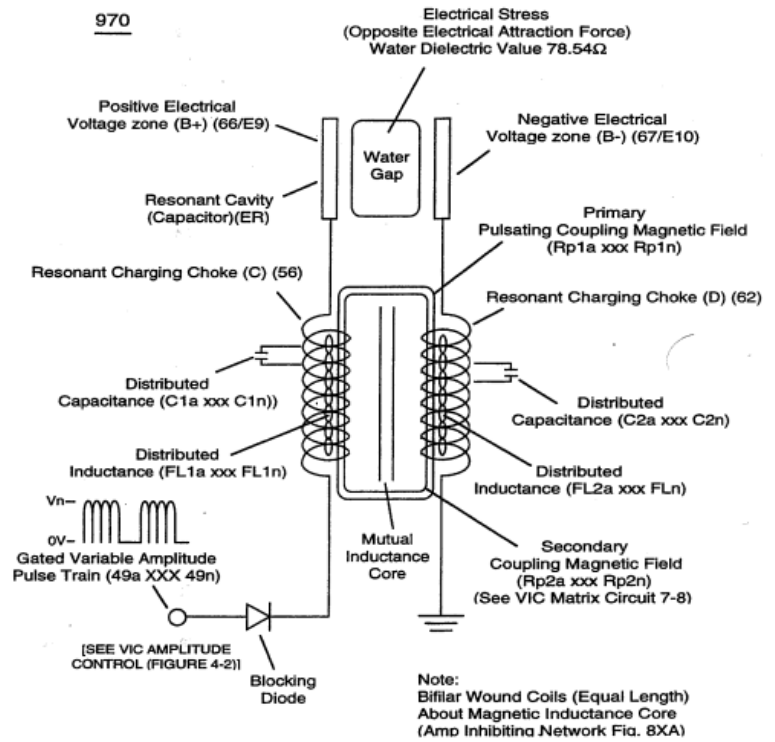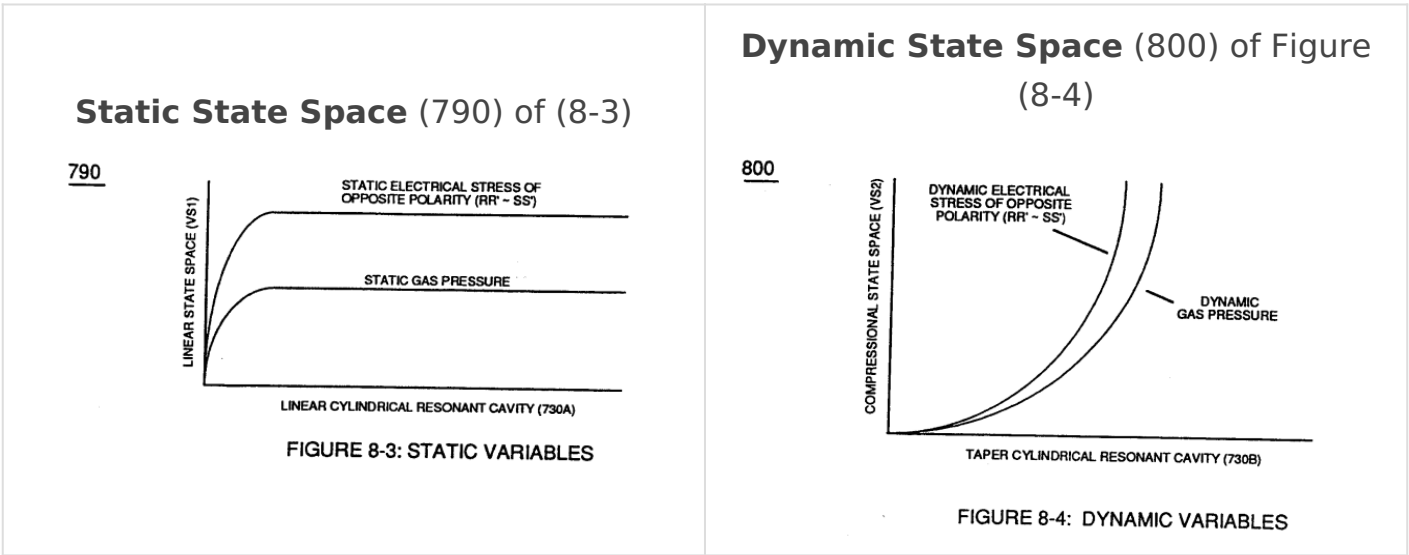(Amp Inhibiting Network Fig. 8XA)

FIGURE 10-1: VOLTAGE INTENSIFIER CIRCUIT

The programmable pulse-frequency (49a xxx 49n) of Figure (10-1) input is simply adjusted to tune-in to the dielectric property of the **Water Molecule**.

The resultant **Dynamic Electrical Charging Effect** (612) of Figure (8-1) acts as a progressive energy enhancer (**Energy Priming Stage**) (500) of Figure (5-1)

Dynamic Electrical Charging Effect (612) of Figure (8-1)

(B) DYNAMIC VOLTAGE STIMULATION

FIGURE 8-1: ELECTRICAL CHARGING STAGE

Energy Priming Stage (500) of Figure (5-1)

FIGURE 5-1: HYDROGEN ENERGY BALANCE
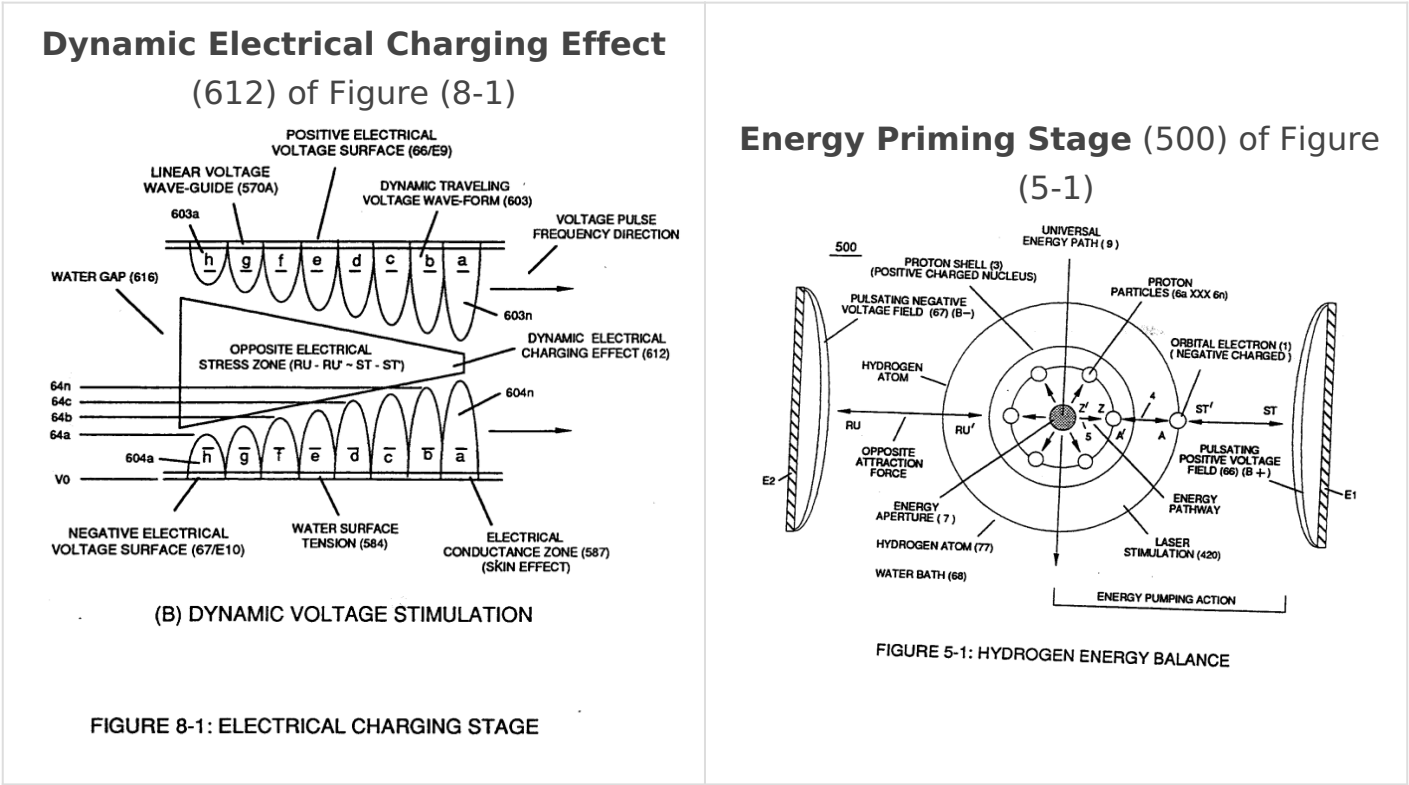
when **Static State Space** (790) of (8-3) is configured to **Dynamic State Space** (800) of Figure (8-4), as so illustrated in WFC memo (427) titled "**Voltage Wave-Guide**"

Static State Space (790) of (8-3)

FIGURE 8-3: STATIC VARIABLES

Dynamic State Space (800) of Figure (8-4)

FIGURE 8-4: DYNAMIC VARIABLES

... whereby, the **Voltage Wave-Guides** forms **Water Gap** (Cp).

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