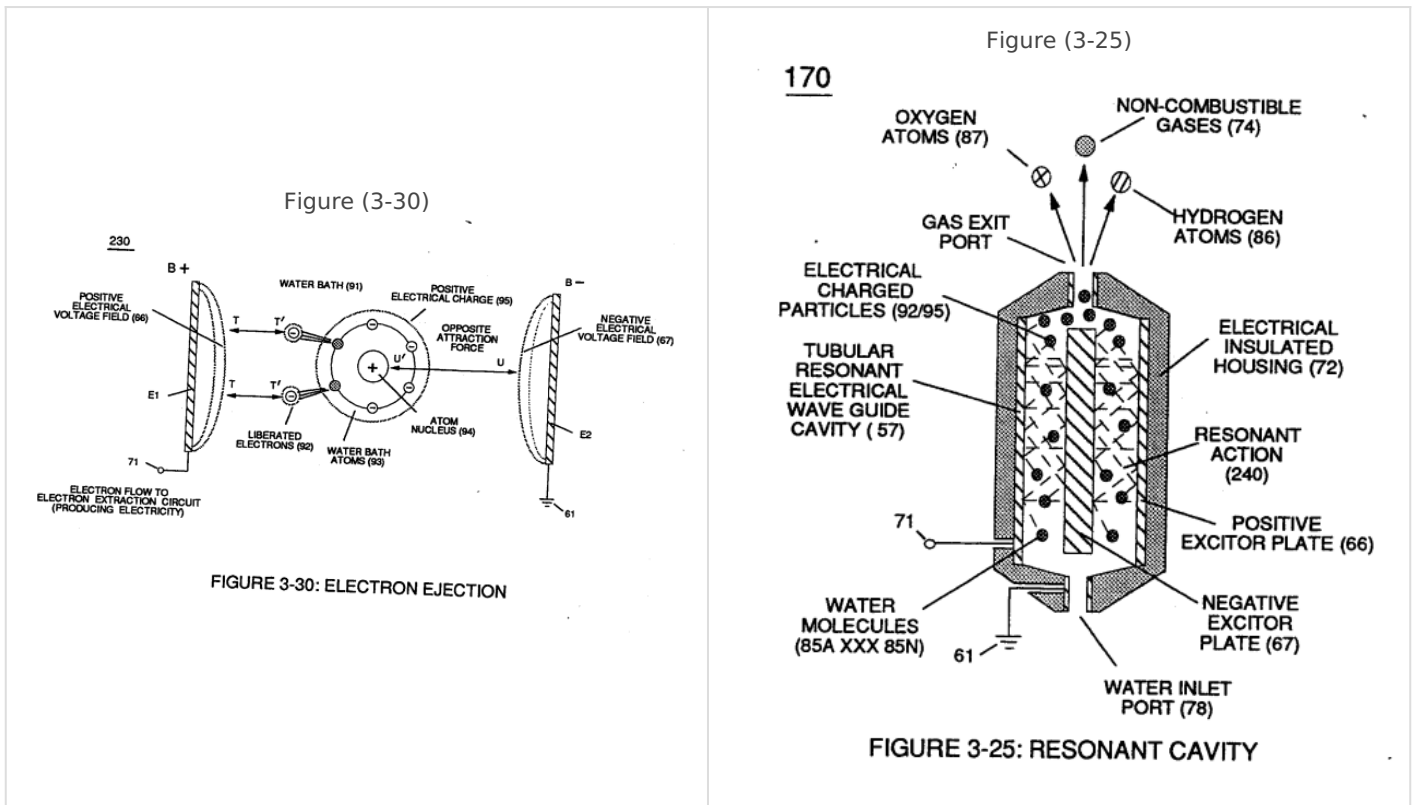


# Resonant Action

Subjecting and exposing **water molecule** (85) to even **higher voltage levels** (xxx Vn) (*up to and beyond several thousand volts*) causes **water bath** (91) of Figure (3-30) as to Figure (3-25) to go into a state of ionization by allowing **opposite polarity forces** (TT') and (UU') to eject one or more **electrons** (92a xxx 92n) from **water bath atoms** (93).



**Intensified electrical attraction force** (TT') causes dislodged **negative charged electrons** (92) to migrate to **positive voltage-plate** (E1) while **electrical attraction force** (UU') causes **positive charged atom nucleus** (94) to travel toward **negative voltage-plate** (E2).

Applied **electrical attraction force** (TT') and (UU') always being of **equal voltage intensity** but **opposite in electrical polarity** as **voltage amplitude** (65) is attenuated.

Replication of **higher voltage forces** (TT') and (UU') during pulsing operations causes a continued release of other **electrons** (92a xxx 92n) from other **water bath atoms** (93a xxx 93n) which, in practice, increases electrical charges of **water bath** (91) since **water bath** (91) is a dielectric liquid.

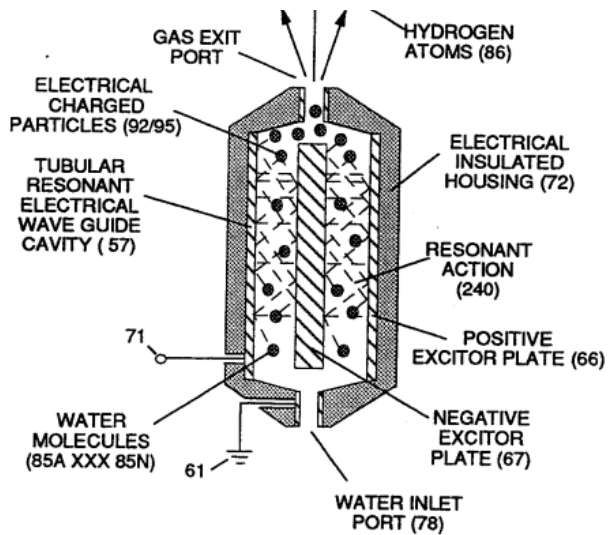


FIGURE 3-25: RESONANT CAVITY

**Water bath atoms** (93a xxx 93n) having missing

**electrons** (92) take-on a **positive electrical charge** (95) which is subject to and moved by negative electrical force (UU'); whereby, the liberated and free floating **negative charge electrons** (92) are subject to and moved by **positive electrical force** (TT').

Applied together, **electrical forces** (TT') and (UU'), now, causes these moving electrically charged particles to superimpose a **physical impact** unto **electrical polarization process** (160), as shown in (170) of Figure (3-25)

... thereby, increasing **gas-yield** (88) still further.

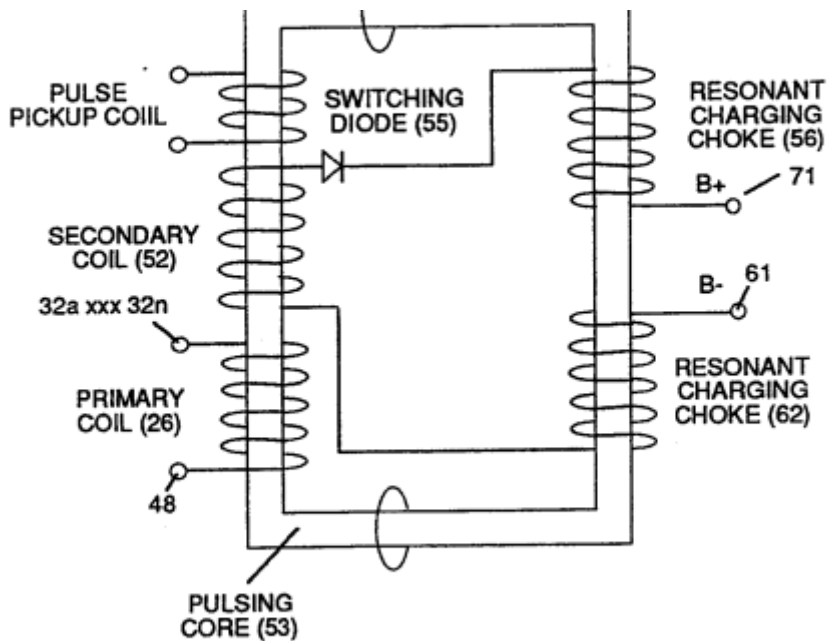


FIGURE 3-23 : PULSING CORE CONFIGURATION

By attenuating **voltage**

**amplitude** ( $V_o \times Y_n$ ) in conjunction with **pulse-width** ( $65a \times 65n$ ) allows **voltage intensifier circuit** (190) of Figure (3-23) to tune-in and match the resonant characteristics or resonant frequency of **water bath** (91) since **water bath** (91) always maintains its dielectric properties during pulsing operations.

At resonance, **electrical polarization process** (160) interacts uniformly with liberated **charged particles** (92/95) of Figure (3-25) to obtain a even **higher gas-yield** (88) at **maximum voltage deflection** ( $\times \times \times V_n$ ).

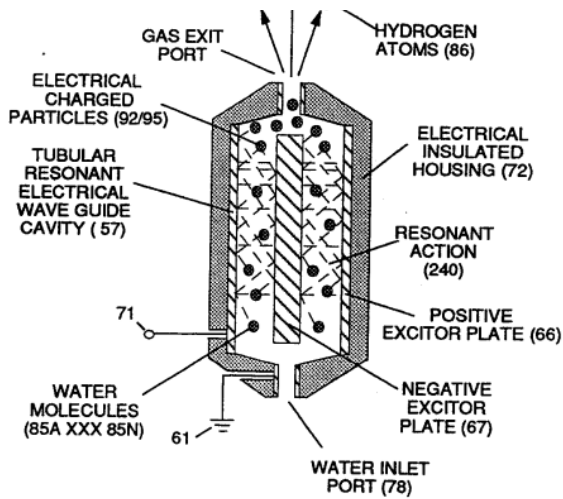


FIGURE 3-25: RESONANT CAVITY

The **established resonant frequency** is most

generally in the audio range from 1 kHz up to and beyond 10 kHz; and is dependent upon the amount of contaminants in **natural water**.

Oscillating and superimposing **electrically charged particles** unto the **Electrical Polarization process** at a given pulse-frequency is, now, herein called "**Resonant Action**", as illustrated in (240) of Figure (3-25).

To reach **maximum gas-yield (88) resonant cavity (170)** of Figure (3-25) is shaped into a **tubular structure** (typically 0.50 inch diameter tube inserted into 0.75 inch diameter tube having a .0625 concentric air-gap 3 inches long) which functions as a longitudinal wave-guide to enhance particle movement in a lateral or angular displacement to applied voltage fields (66/67).

**Insulated housing (72)** prevents **voltage coupling to water bath (68)** which allows **applied voltage amplitude** (xxx Vn) to remain constant across **water molecules (85a xxx 85n)**

... stabilizing gas production during voltage stimulation (65), as shown in (120) of Figure (3-24).

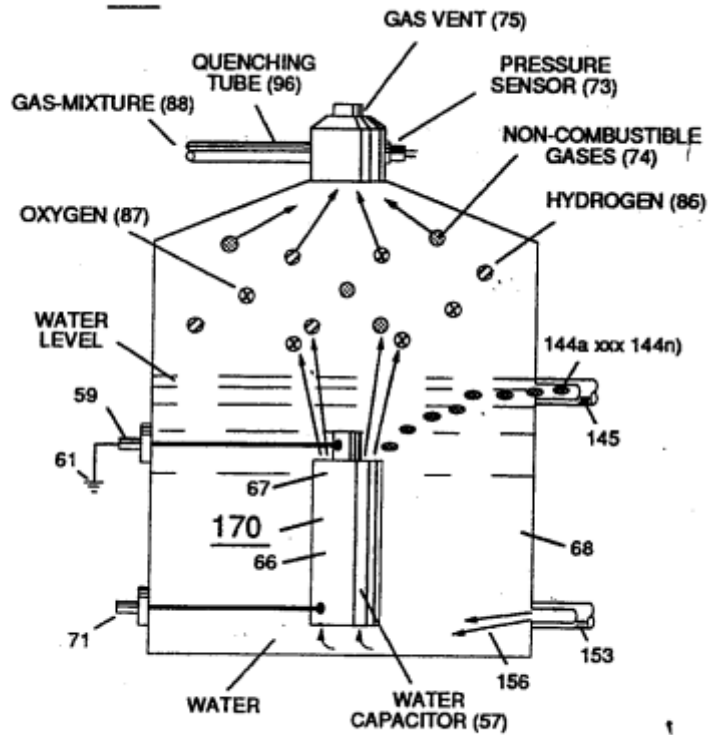


FIGURE 3-24: FUEL CELL

To further prevent voltage fluctuation during resonant action, **Phase Lock Loop** technique of **Pulse Indicator circuit** (110) is utilized during pulsing operations.

The resultant **fuel-gas** (88) is, now, transferred through **Quenching Tube** (96) of Figure (3-41) to, through and beyond **Fuel Injectors** (36) of Figure (3-1) for Hydrogen gas utilization.

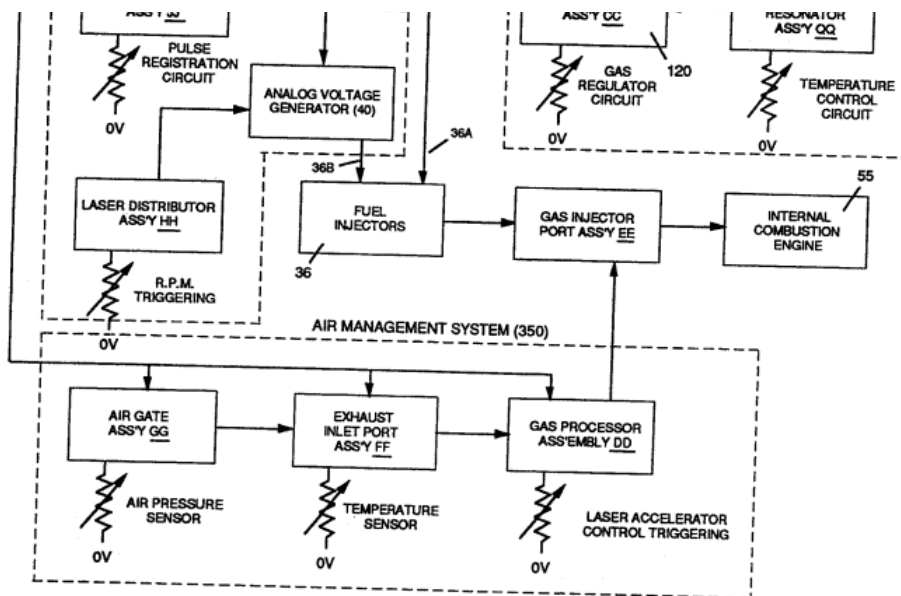


FIGURE 3-1: HYDROGEN GAS MANAGEMENT SYSTEM

In cases where applied

voltage amplitude is to remain constant while promoting **Resonant Action** during control-state, **incoming pulse train** (64a xxx 64n) is varied independent of voltage amplitude to attenuate **voltage intensity** (66/67) which, in turn, effects gas production.

In other applications, **Voltage amplitude** (66/67) in direct relationship to **pulse-train** (64a xxx 64n) may be varied together in a progressive manner to further control gas production. Or pulse-train (64a xxx 64n) can remain constant while voltage amplitude is varied.

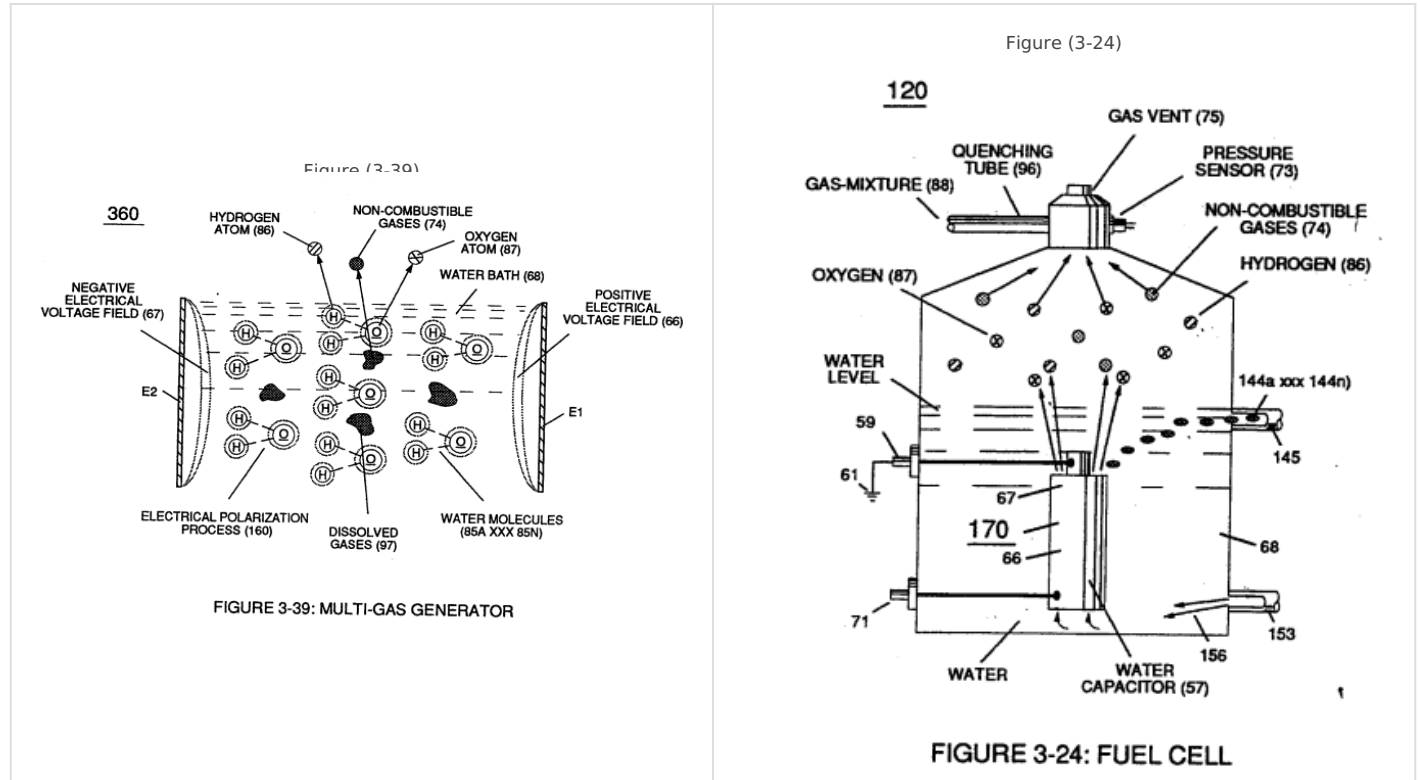
In all cases, **Resonant Action** is being promoted to produce hydrogen gas on demand.

In terms of Longevity, **voltage zones** (E1/E2) are composed of or made of stainless steel T304 material which is chemically inert to hydrogen, oxygen, and ambient air gases (*dissolved gases in water*) being liberated from **water bath** (68) during **voltage stimulation** (65).

Under actual certified laboratory testing stainless steel T304 life expectancy ( *material decomposition*) is .0001 per year since **voltage** (65) is a physical force, setting up a non-chemical environment since amps consumption is being restricted to a minimum and "no" electrolyte is added to **water bath** (68).

In practice, **stainless steel voltage plates** (E1/E2) physically forms **voltage zones** (66/67) regardless of geometric shape or configuration of **resonant cavity** (170).

Under normal gas ignition or gas combustion process, released **Fuel-Gases** (88) of Figure (3-39) as to Figure (3-24) nets a **thermal explosive energy yield** (gtnt) of approximately 2 1/2 times greater than gasoline.



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