

Voltage to Amp Differential Ratio

Opposite polarity **Voltage Wave burst** (1010) of Figure (10-5) as to **Dynamic Voltage Stimulation** (770B) of Figure (8-1) is simply produced when **Programmable Variable Pulse-Width Pulse-Train Waveform** (49a xxx 49n) is allowed to be electrically transmitted through and beyond **Resonant Charging Chokes Stages** (56/62a xx 56/62n + SS56/62a xxx SS56/62n) of Figure (10-4) that are not only electrically connected in **sequential order** but likewise magnetically linked by **Inductance Coupling field** (511/512a xxx 511/512n), as so pictorially illustrated in (580) of Figure (6-1).

Voltage Rippling Effect (1010) of
Figure (10-5)

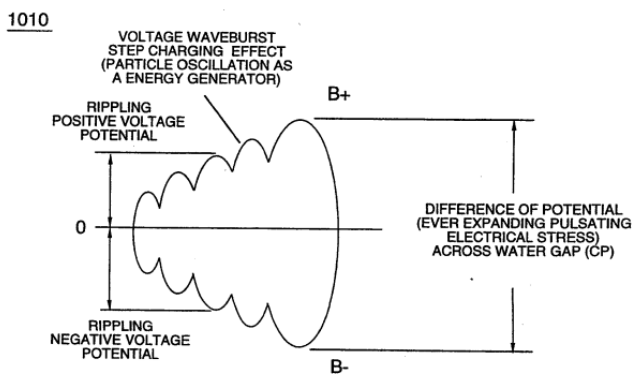
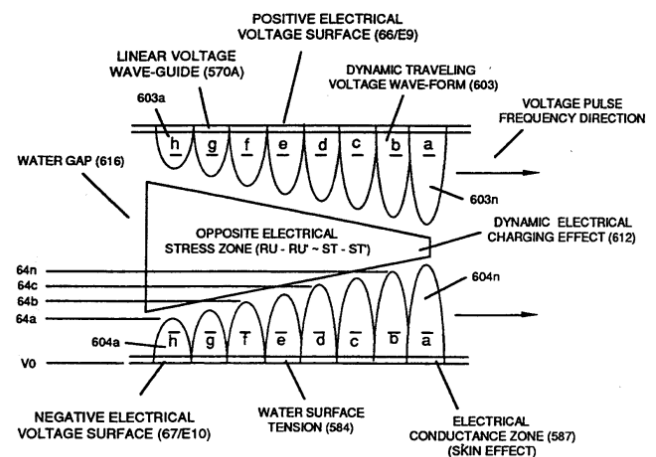


FIGURE 10-5: OPPOSITE VOLTAGE CHARGING EFFECT

Dynamic Voltage Stimulation (770B)
of Figure (8-1)

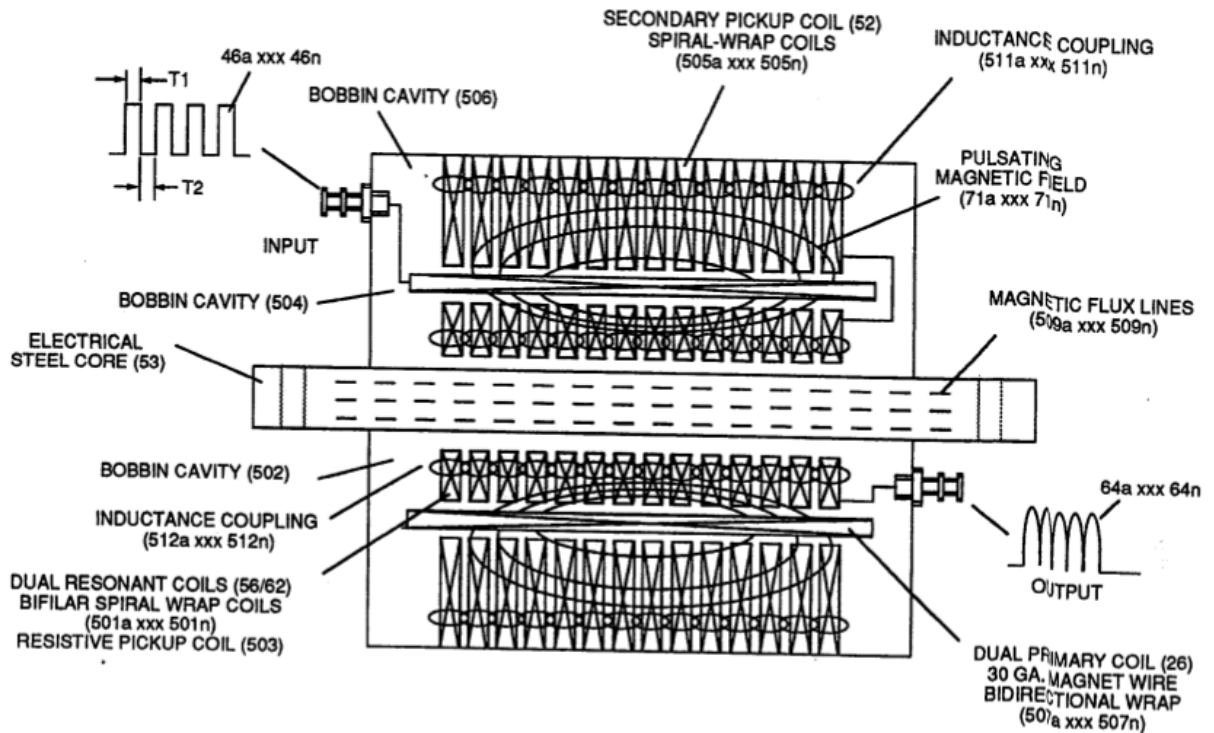


(B) DYNAMIC VOLTAGE STIMULATION

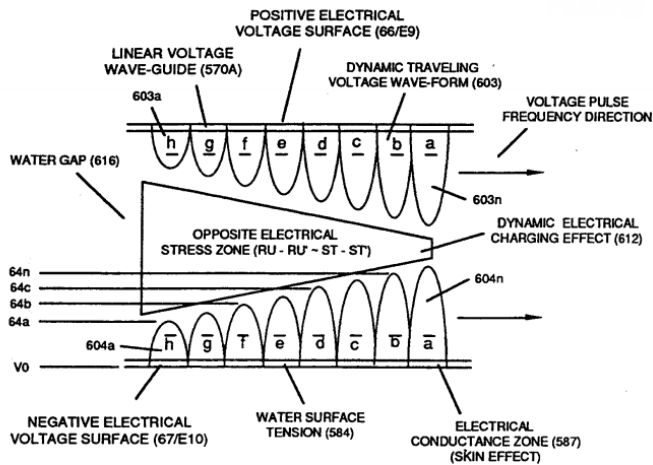
FIGURE 8-1: ELECTRICAL CHARGING STAGE

(580) of Figure (6-1)

580



8-1: (VIC) COIL ASSEMBLY



(B) DYNAMIC VOLTAGE STIMULATION

FIGURE 8-1: ELECTRICAL CHARGING STAGE

The resultant **ever increasing** pulsating

opposite electrical voltage fields ($603/604a \times \times \times 603/604n$) of Figure (8-1) having superimposed thereon counter opposing **Rippling Voltage-Surfaces** ($64/B+a \times \times \times$

64/B-n) [**Dynamic Electrical Charging Effect** (612) of Figure (8-1B)], now, set ups, causes, and applies **ever increasing** (*rubberbanding effect*) **Pulsating Opposite Electrical Stress** (RU-RU' - ST-ST') across **Water Gap** (Cp)

... encouraging "**Particle Oscillation**" as a "**Energy Generator**" by way of pulsating "**Electrical Stress**" as the combustible gas atom particles of the water molecule undergo "**Particle Deflection**" farthest from the point of "**State of Equilibrium**" and returning back to "**Stable State of Equilibrium**" during-pulse off-time (T2) for repeated "**Snapping Action**" (*Rubberbanding effect*) in accordance with bi-polar **Voltage Rippling Effect** (1010) of Figure (10-5), as so illustrated in (280) of Figure (3-35).

Voltage Rippling Effect (1010) of Figure (10-5)

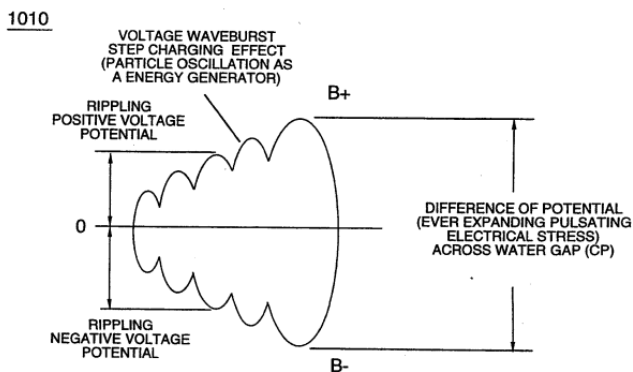


FIGURE 10-5: OPPOSITE VOLTAGE CHARGING EFFECT

(280) of Figure (3-35)

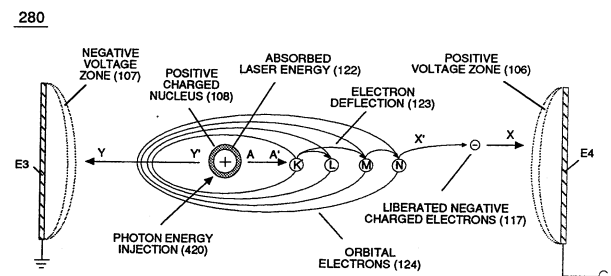


FIGURE 3-35: LASER INTERACTION

The greater the **Electrical Stress** (RU-RU' a xxx ST -ST'n) applied (64B+/64B-a xxx 64B+/64B-), the greater amount of thermal explosive energy (16/gtnta xxx 16/gtntn) of Figure (6-2) as to (70) of Figure (4-5) is released from **Resonant Water Gap** (Cp) (970) of Figure (10-1), as further illustrated in (70) of Figure (4-5).

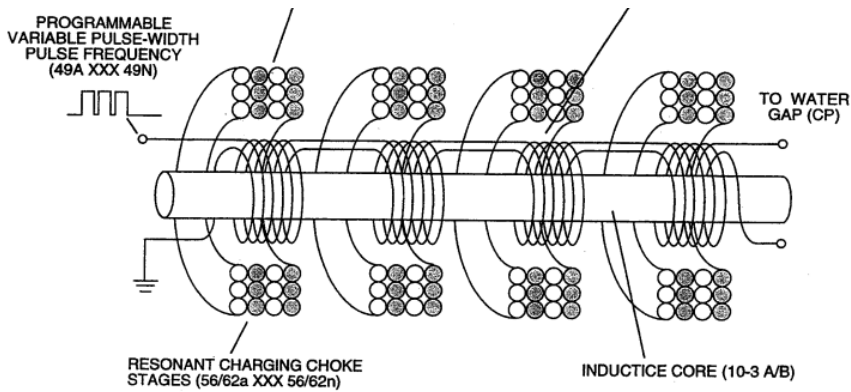


FIGURE 10-4: DUAL-LAYERED MULTI - SPOOL CONFIGURATION

Increasing energy-yield

(16/gtnt) still further (xxx 16/gtntn1+ 16/gtntn2 + 16/gtntn ... etc.) is accomplished by increasing the number of **Resonant Charging Choke Stages** (xxx 56/62n + 56/62n1 + 56/62n2 + 56/62n ... etc. -S- xxx SS56/62n + SS56/62n1 + SS56/62n2 + SS56/62n ... etc.) of Figure (10-4) in "**Sequential Order**" (-S-) since the total number of **Multi-Coil Magnet** bifilar coils (56/62a xxx 56/62n) serially electrically connected together are sequentially electrically linked to an equal number of serially electrically aligned **Stainless Steel Resonant Coils** (SS/56/62a xxx SS/56/62n)

... allowing each/both **bifilar coil assembly** (56/62a xxx 56/62n -S- SS56/62a xxx SS56/62n) to be electrically and magnetically energized **in the same progressive direction** toward **Water Gap** (Cp) and away from blocking diode (55) of Figure (3-34) as to Figure (10-1) and Figure (10-3)

Figure (10-1)

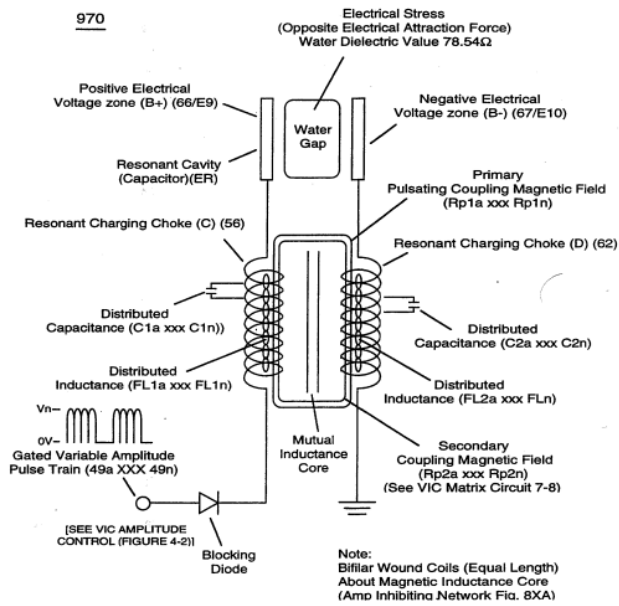
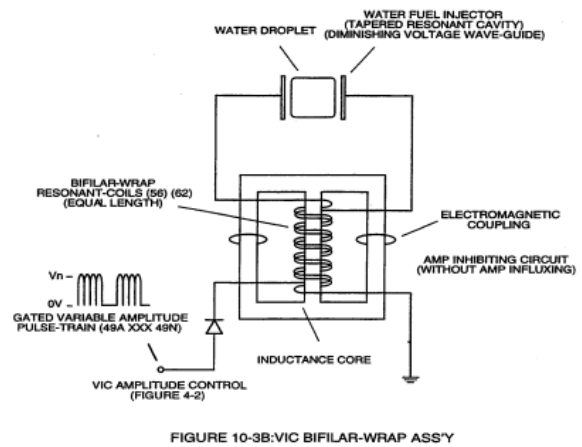
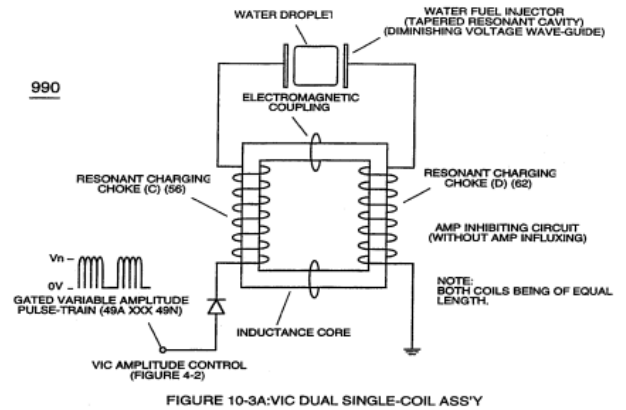


Figure (10-3)



keeping amp-surge (inhibiting amp flow) to a minimal level [See **Voltage Performance Graph** (750) of Figure (7-14)] while enhancing **Voltage Potential of Electrical Stress** (64/RU'a xxx 64/ST-ST'n) as additional **Dual Choke Coils** (56/62 _SS56/62) are included in the stacked coil-array forming **Voltage Intensifier Circuit** (970) of Figure (10-1) as to (620) of figure (7-1)

blocking diode (55) of Figure (3-34)

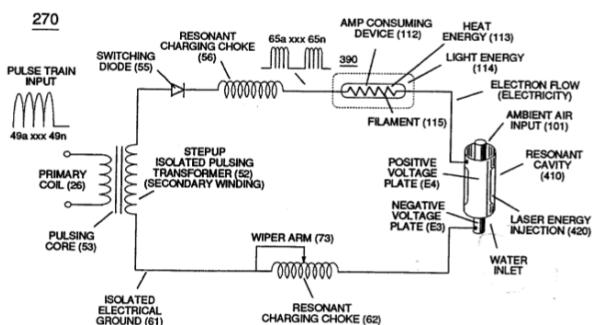
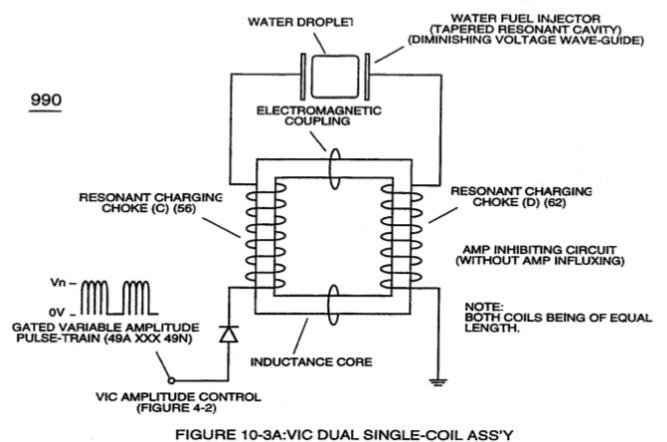


Figure (10-3A)



Voltage Performance Graph (750) of Figure (7-14)

750

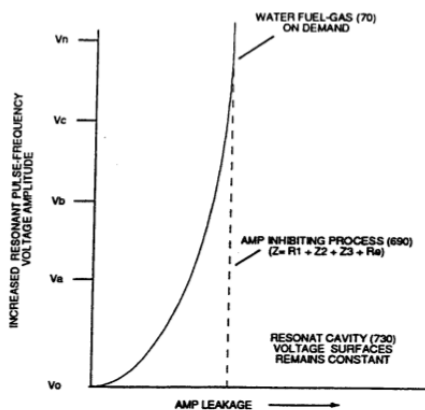
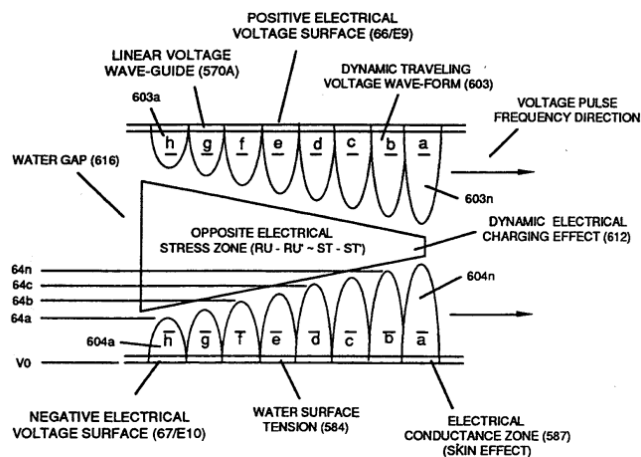


FIGURE 7-14: RESONANT CAVITY WATER-FUEL INJECTION

Figure (10-3B)



(B) DYNAMIC VOLTAGE STIMULATION

FIGURE 8-1: ELECTRICAL CHARGING STAGE

Voltage Intensifier Circuit (970) of Figure (10-1)

970

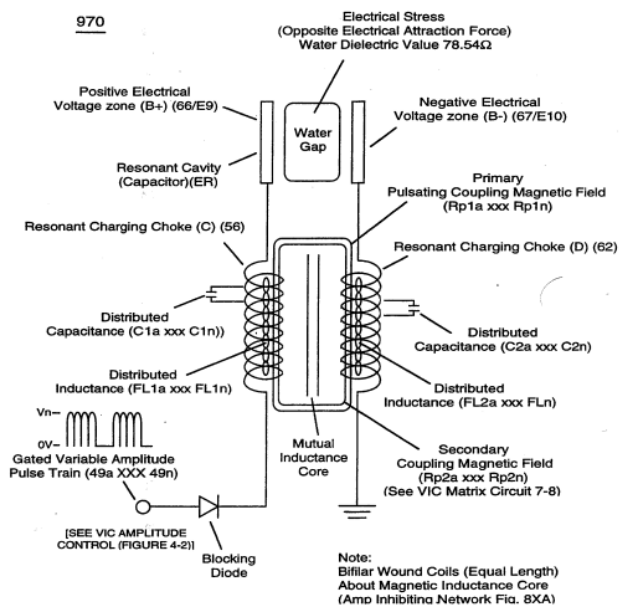


FIGURE 10-1: VOLTAGE INTENSIFIER CIRCUIT

(620) of figure (7-1)

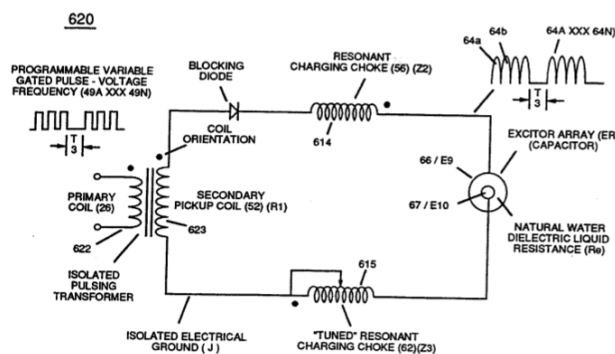
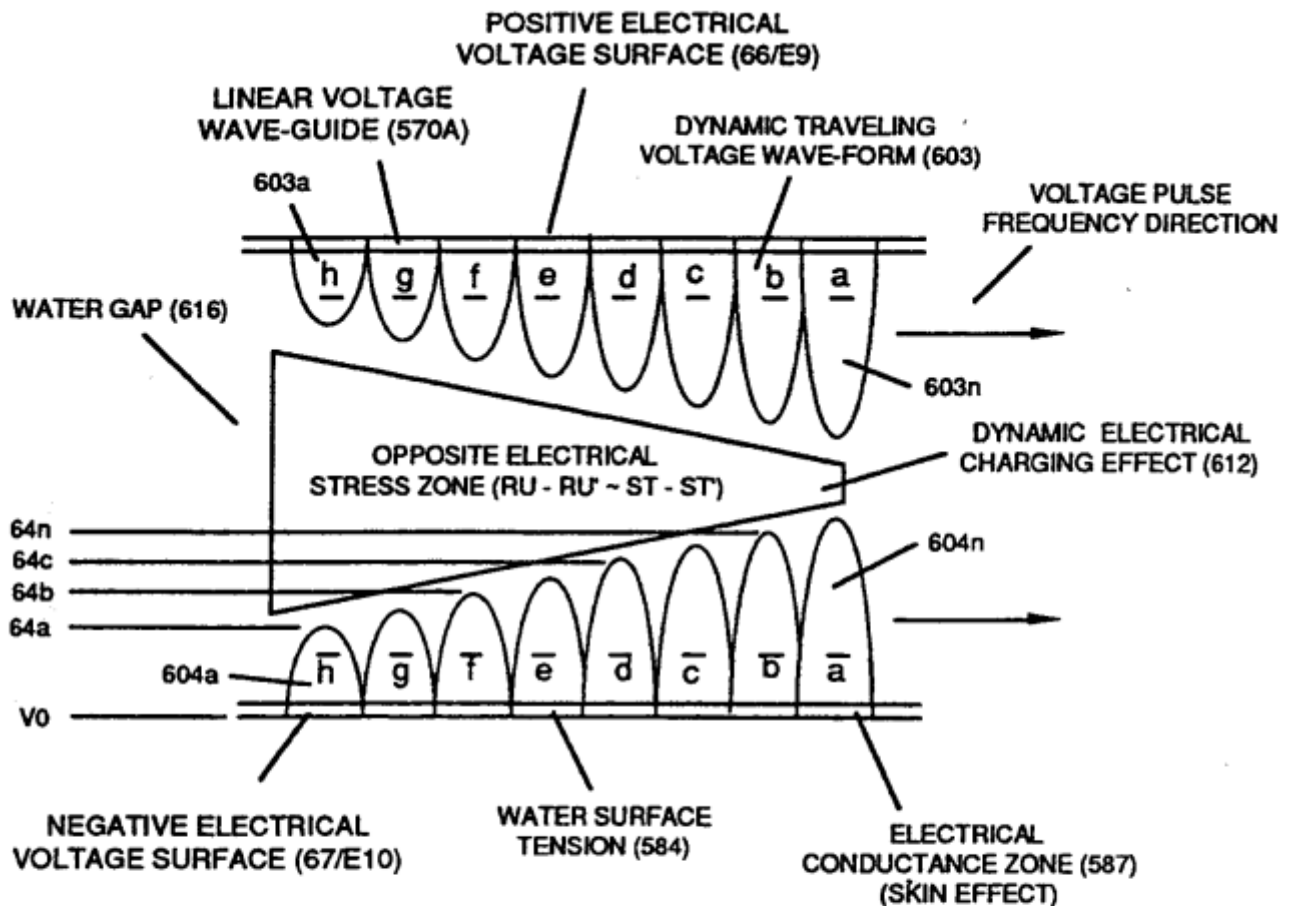


FIGURE 7-1: VIC IMPEDANCE NETWORK

... see **Dynamic Voltage Waveform** (770) of Figure (8-1), once again.



(B) DYNAMIC VOLTAGE STIMULATION

FIGURE 8-1: ELECTRICAL CHARGING STAGE

In Retrospect, the use of **Stainless Steel** composite coil-wire (430F/FR) consists of both inductance and resistive properties (typically .0048 ohms per foot) which when combined together in metallurgical form aids amp restriction beyond the singularly use of self-inductance magnet (Copper) coil-wire having a lower resistive value.

Stainless Steel bifilar Coil-Stage Assembly (SS56/62a xxx SS56/62n) is electrically placed between **Magnet Coil-Stage Assembly** (56/62a xxx 56/62n) and **Water Gap** (Cp) to obtain optimum **Voltage to Amp Differential Ratio** ($V_{\text{highest}}:A_{\text{lowest}}$ ratio).

Together, **Coil Stages** (56/62a xxx 56/62n + SS56/62a xxx SS56/62) added/stacked sequentially into a single overall coil-array assembly (990A/B) of Figure (10-3) forms

Amp Inhibiting Network (Figure 8XA) as to (970) of Figure (10-1) (hereinafter called **VIC Multi-Coil Spool Assembly**).

The magnet **Coil-Wire** (56/62) is best suited for **Voltage** inducement while the inductance/capacitance/resistance properties of **Stainless Steel coil-wire** (SS56-SS62) is appropriately used to **restrict electron movement** beyond the self-inductance of each energized coil when elevated voltage levels (*up to beyond 40 kilovolts*) are to be reached/obtained without experiencing any appreciable amount of "**Amp Influxing**."

Generally, magnet coil-wire length is longer than the Stainless steel coil-wire length and magnet bifilar-coil (56/62) is placed on top of **Stainless Steel bifilar-coil** (SS56/62) to maximize mutual inductance coil-field (R_{p2}) (adding $R_{p1} + R_{p2}$) of (690) of Figure (7-8) to cause coil capacitance ($C_{da} \times \times \times C_{dn}$) to help maintain and even increase pulse voltage amplitude ($\times \times \times V_n + V_{n1} + V_{n2} + V_n \dots$ etc.) while the resistive value (R_{s2}) of SS Coil-Wire (SS56/62) performs the work of further resisting the flow of amps not inhibited by both self-Inductance fields ($R_{p1} + R_{p2}$), as so illustrated in (690) of Figure (7-8).

(690) of Figure (7-8)

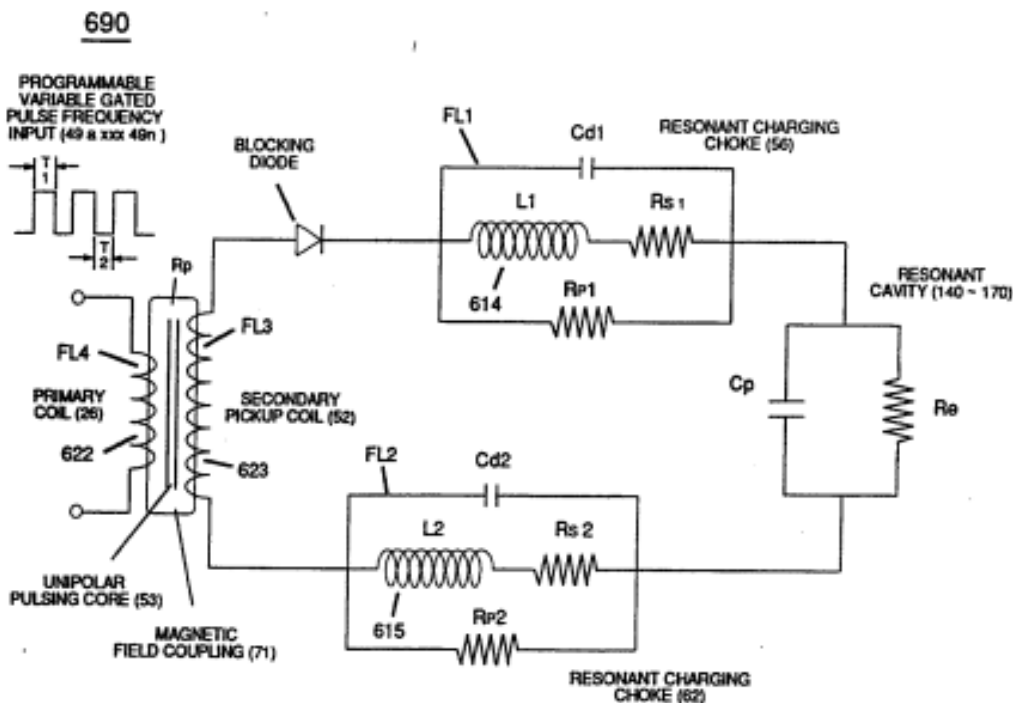


FIGURE 7-8: VIC MATRIX CIRCUIT

In all cases, bifilar coils (56/62 - SS56/62) are electromagnetically orientated **in the same direction**.

In terms of operability, electrically flexing (**Particle Oscillation**) the combustible atoms of the water molecule as a "**Energy Generator**" by way of opposite voltage polarity is extremely economical since voltage is not consumed in an electronic circuit.

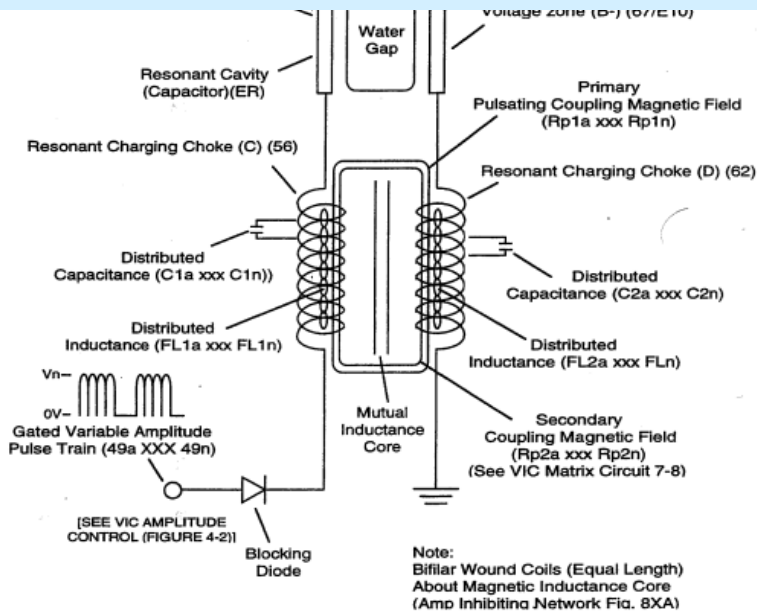


FIGURE 10-1: VOLTAGE INTENSIFIER CIRCUIT

Amp Inhibiting Circuit (970) of

Figure (10-1) restricts/inhibits amp flow to a minimal level while elevating "**Difference of Potential**" to the highest possible level.

The greater the "**Difference of Potential**" (in this case, electrical stress) the greater amount of work is performed

... thereby, being in compliance with the **Laws of Physics** since atoms are the source of all energy in our physical universe and atoms are directly responsive to / stimulated by external electrical forces.