Voltage to Amp Differential Ratio

Opposite polarity **Voltage Wave burst** (1010) of Figure (10-5) as to **Dynamic Voltage Stimulation** (770B) of Figure (8-1) is simply produced when **Programmable Variable Pulse-Width Pulse-Train Waveform** (49a xxx 49n) is allowed to be electrically transmitted through and beyond **Resonant Charging Chokes Stages** (56/62a xx 56/62n + SS56/62a xxx SS56/62n) of Figure (10-4) that are not only electrically connected in **sequential order** but likewise magnetically linked by **Inductance Coupling field** (511/512a xxx 511/512n), as so pictorially illustrated in (580) of Figure (6-1).

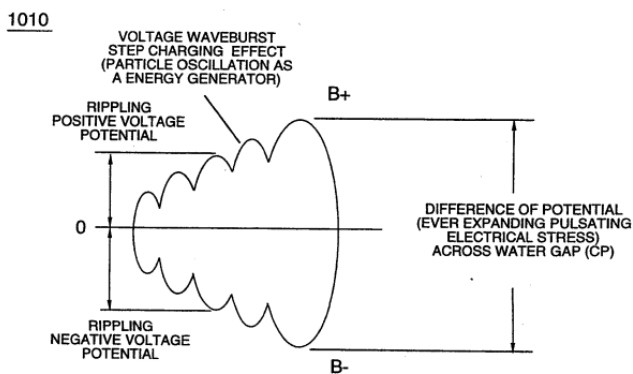
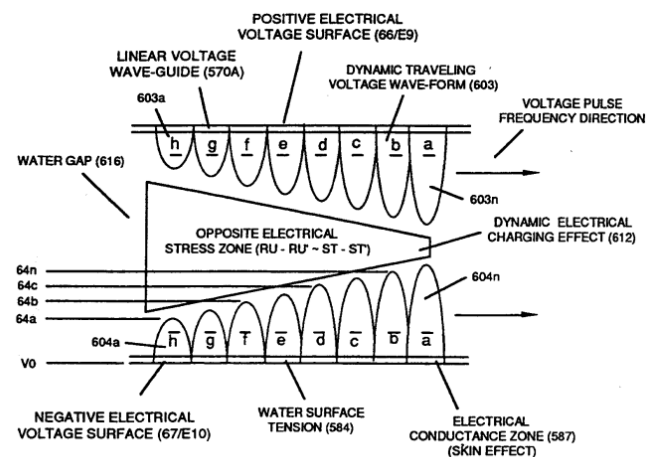**Voltage Rippling Effect** (1010) of Figure (10-5)

FIGURE 10-5: OPPOSITE VOLTAGE CHARGING EFFECT

Dynamic Voltage Stimulation (770B) of Figure (8-1)
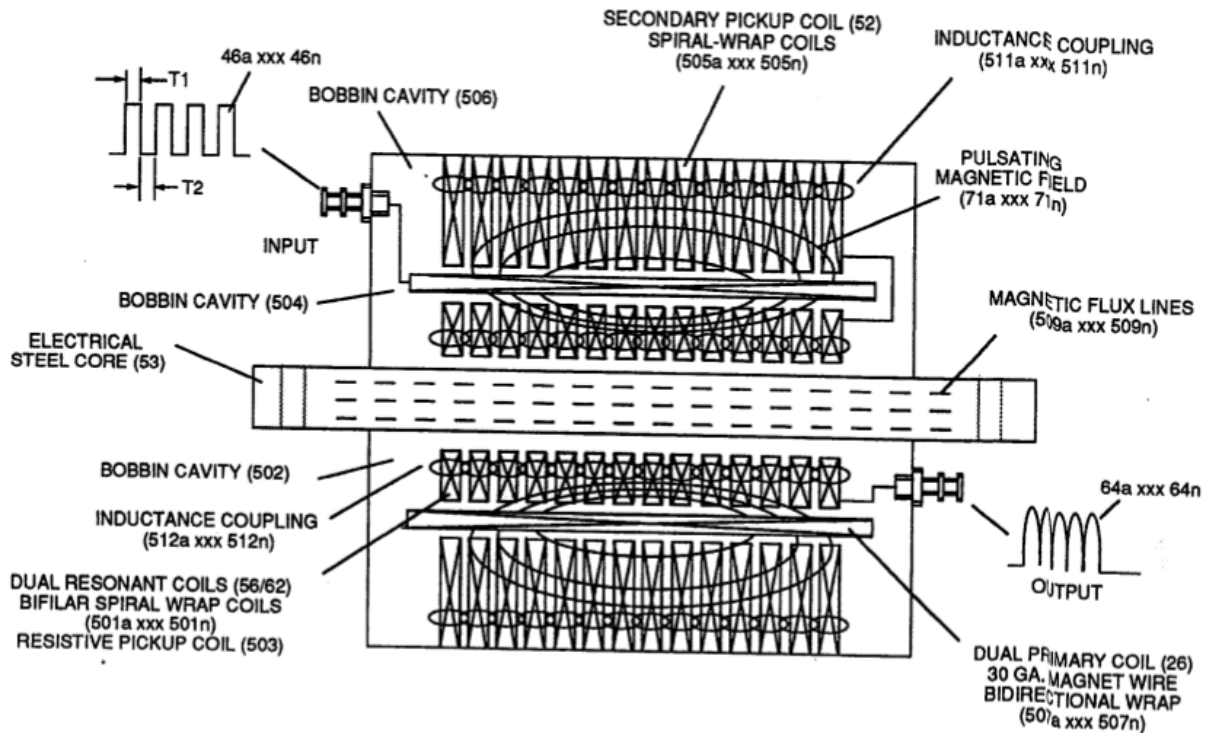
(B) DYNAMIC VOLTAGE STIMULATION
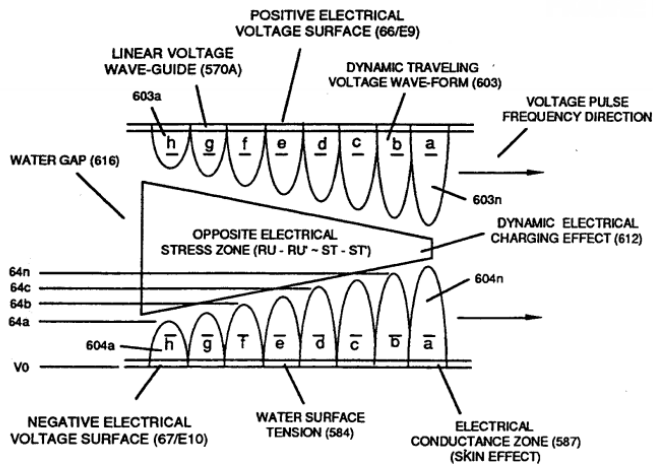
FIGURE 8-1: ELECTRICAL CHARGING STAGE

580

FIGURE 6-1: (VIC) COIL ASSEMBLY

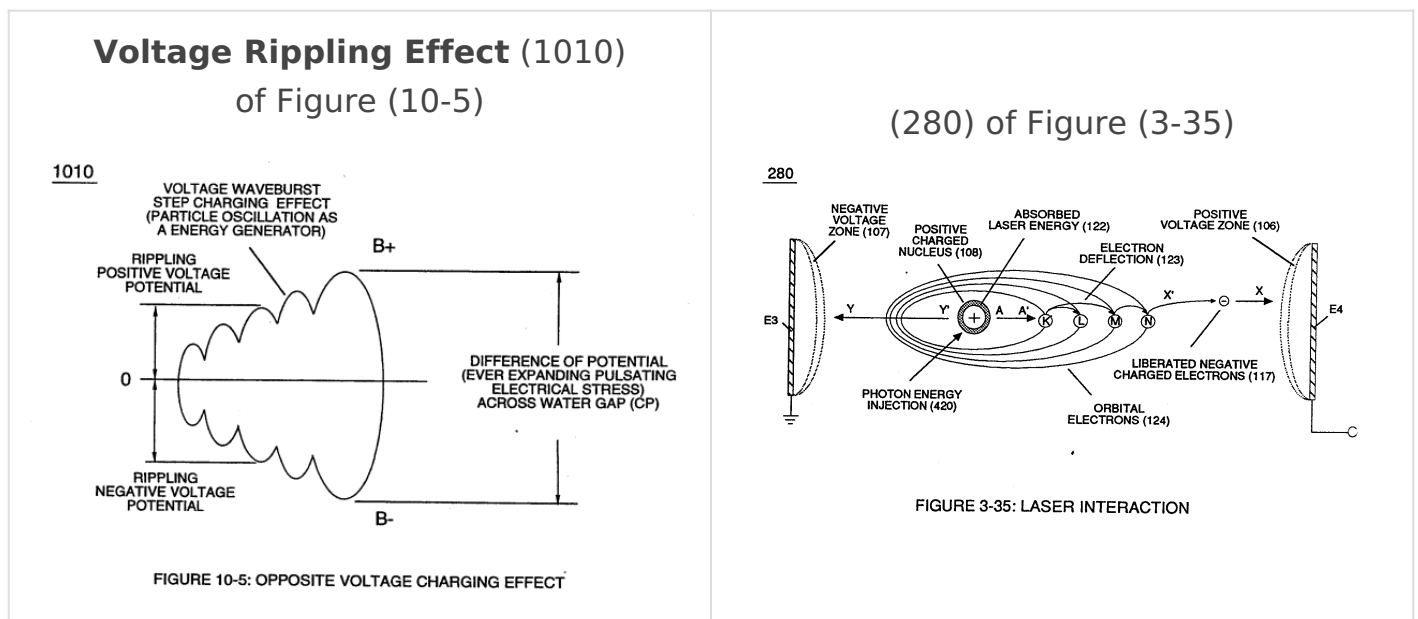(B) DYNAMIC VOLTAGE STIMULATION

FIGURE 8-1: ELECTRICAL CHARGING STAGE

The resultant **ever increasing** pulsating

opposite electrical voltage fields (603/604a xxx 603/604n) of Figure (8-1) having superimposed thereon counter opposing **Rippling Voltage-Surfaces** (64/B+a xxx

64/B-n) [**Dynamic Electrical Charging Effect** (612) of Figure (8-1B)], now, set ups, causes, and applies **ever increasing** *(rubberbanding effect)* **Pulsating Opposite Electrical Stress** (RU-RU' - ST-ST') across **Water Gap** (Cp)

... encouraging "**Particle Oscillation**" as a "**Energy Generator**" by way of pulsating "**Electrical Stress**" as the combustible gas atom particles of the water molecule undergo "**Particle Deflection**" farthest from the point of "**State of Equilibrium**" and returning back to "**Stable State of Equilibrium**" during-pulse off-time (T2) for repeated "**Snapping Action**" *(Rubberbanding effect)* in accordance with bi-polar **Voltage Rippling Effect** (1010) of Figure (10-5), as so illustrated in (280) of Figure (3-35).

Voltage Rippling Effect (1010) of Figure (10-5)

1010

FIGURE 10-5: OPPOSITE VOLTAGE CHARGING EFFECT

(280) of Figure (3-35)

280

FIGURE 3-35: LASER INTERACTION

The greater the **Electrical Stress** (RU-RU' a xxx ST -ST'n) applied (64B+/64B-a xxx 64B+/64B-), the greater amount of thermal explosive energy (16/gtnta xxx 16/gtntn) of Figure (6-2) as to (70) of Figure (4-5) is released from **Resonant Water Gap** (Cp) (970) of Figure (10-1), as further illustrated in (70) of Figure (4-5).

FIGURE 10-4: DUAL-LAYERED MULTI - SPOOL CONFIGURATION

Increasing energy-yield

(16/gtnt) still further (xxx 16/gtntnl+ 16/gtntn2 + 16/gtntn ... etc.) is accomplished by increasing the number of **Resonant Charging Choke Stages** (xxx 56/62n + 56/62n 1+ 56/62n2 + 56/62n ... etc. -S- xxx SS56/62n + SS56/62nl + SS56/62n2 + SS56/62n ... etc.) of Figure (10-4) in "**Sequential Order**" (-S-) since the total number of **Multi-Coil Magnet** bifilar coils (56/62a xxx 56/62n) serially electrically connected together are sequentially electrically linked to an equal number of serially electrically aligned **Stainless Steel Resonant Coils** (SS/56/62a xxx SS/56/62n)

... allowing each/both **bifilar coil assembly** (56/62a xxx 56/62n -S- SS56/62a xxx SS56/62n) to be electrically and magnetically energized **in the same progressive direction** toward **Water Gap** (Cp) and away from blocking diode (55) of Figure (3-34) as to Figure (10-1) and Figure (10-3)

Figure (10-1)

970

Electrical Stress
(Opposite Electrical Attraction Force)
Water Dielectric Value 78.54Ω

Positive Electrical
Voltage zone (B+) (66/E9)

Negative Electrical
Voltage zone (B-) (67/E10)

Water Gap

Resonant Cavity
(Capacitor)(ER)

Primary
Pulsating Coupling Magnetic Field
(Rp1a xxx Rp1n)

Resonant Charging Choke (C) (56)

Resonant Charging Choke (D) (62)

Distributed
Capacitance (C1a xxx C1n))
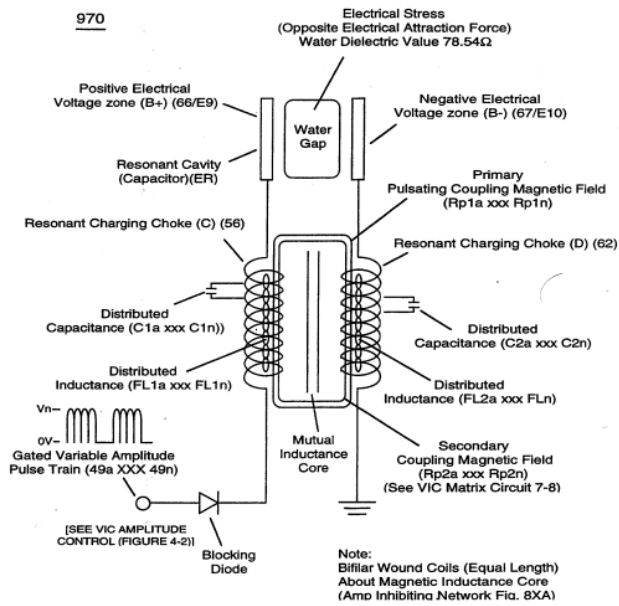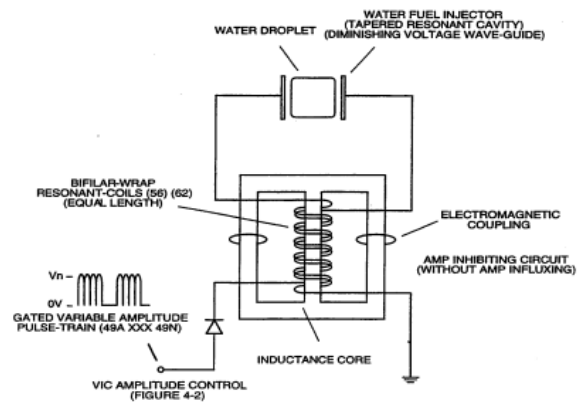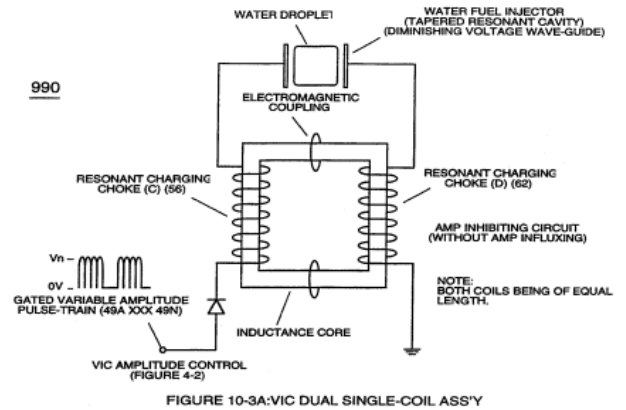
Distributed
Capacitance (C2a xxx C2n)

Distributed
Inductance (FL1a xxx FL1n)

Distributed
Inductance (FL2a xxx FLn)

Vn—
0V—
Gated Variable Amplitude
Pulse Train (49a XXX 49n)

Mutual
Inductance
Core

Secondary
Coupling Magnetic Field
(Rp2a xxx Rp2n)
(See VIC Matrix Circuit 7-8)

[SEE VIC AMPLITUDE
CONTROL (FIGURE 4-2)]

Blocking
Diode

Note:
Bifilar Wound Coils (Equal Length)
About Magnetic Inductance Core
(Amp Inhibiting Network Fig. 8XA)

FIGURE 10-1: VOLTAGE INTENSIFIER CIRCUIT

Figure (10-3)

990

WATER DROPLET

WATER FUEL INJECTOR
(TAPERED RESONANT CAVITY)
(DIMINISHING VOLTAGE WAVE-GUIDE)

ELECTROMAGNETIC
COUPLING

RESONANT CHARGING
CHOKE (C) (56)

RESONANT CHARGING
CHOKE (D) (62)

AMP INHIBITING CIRCUIT
(WITHOUT AMP INFLUXING)

Vn—
0V—
GATED VARIABLE AMPLITUDE
PULSE-TRAIN (49A XXX 49N)

NOTE:
BOTH COILS BEING OF EQUAL
LENGTH.

INDUCTANCE CORE

VIC AMPLITUDE CONTROL
(FIGURE 4-2)

FIGURE 10-3A:VIC DUAL SINGLE-COIL ASS'Y

WATER DROPLET

WATER FUEL INJECTOR
(TAPERED RESONANT CAVITY)
(DIMINISHING VOLTAGE WAVE-GUIDE)

BIFILAR-WRAP
RESONANT-COILS (56) (62)
(EQUAL LENGTH)

ELECTROMAGNETIC
COUPLING

AMP INHIBITING CIRCUIT
(WITHOUT AMP INFLUXING)

Vn—
0V—
GATED VARIABLE AMPLITUDE
PULSE-TRAIN (49A XXX 49N)

INDUCTANCE CORE

VIC AMPLITUDE CONTROL
(FIGURE 4-2)

FIGURE 10-3B:VIC BIFILAR-WRAP ASS'Y

keeping amp-surge (inhibiting amp flow) to a minimal level [See **Voltage Performance Graph** (750) of Figure (7-14)] while enhancing **Voltage Potential of Electrical Stress** (64/RU-RU'a xxx 64/ST-ST'n) as additional **Dual Choke Coils** (56/62 _ SS56/62) are included in the stacked coil-array forming **Voltage Intensifier Circuit** (970) of Figure (10-1) as to (620) of figure (7-1)
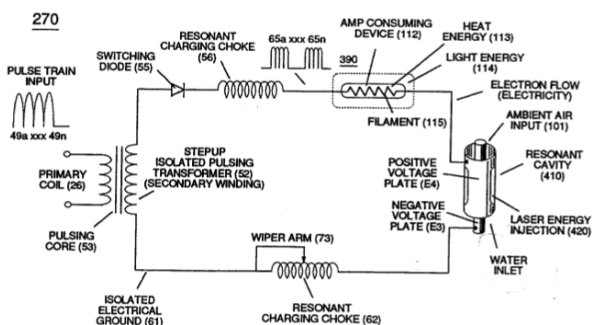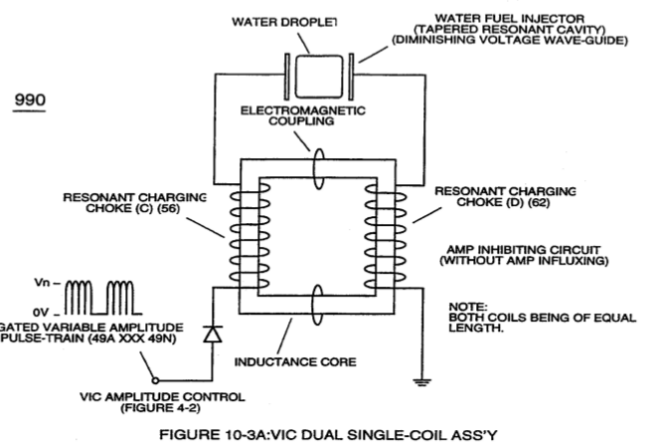
blocking diode (55) of Figure (3-34)

270

RESONANT
CHARGING CHOKE
(56)

65a xxx 65n

AMP CONSUMING
DEVICE (112)

HEAT
ENERGY (113)

SWITCHING
DIODE (55)

LIGHT ENERGY
(114)

PULSE TRAIN
INPUT

390

ELECTRON FLOW
(ELECTRICITY)

49a xxx 49n

FILAMENT (115)

AMBIENT AIR
INPUT (101)

STEPUP
ISOLATED PULSING
TRANSFORMER (52)
(SECONDARY WINDING)

POSITIVE
VOLTAGE
PLATE (E4)

RESONANT
CAVITY
(410)

PRIMARY
COIL (26)

NEGATIVE
VOLTAGE
PLATE (E3)

LASER ENERGY
INJECTION (420)

PULSING
CORE (53)

WIPER ARM (73)

WATER
INLET

ISOLATED
ELECTRICAL
GROUND (61)

RESONANT
CHARGING CHOKE (62)

FIGURE 3-34: ELECTRON EXTRACTION CIRCUIT

Figure (10-3A)

990

WATER DROPLET

WATER FUEL INJECTOR
(TAPERED RESONANT CAVITY)
(DIMINISHING VOLTAGE WAVE-GUIDE)

ELECTROMAGNETIC
COUPLING

RESONANT CHARGING
CHOKE (C) (56)

RESONANT CHARGING
CHOKE (D) (62)

AMP INHIBITING CIRCUIT
(WITHOUT AMP INFLUXING)

Vn—
0V—
GATED VARIABLE AMPLITUDE
PULSE-TRAIN (49A XXX 49N)

NOTE:
BOTH COILS BEING OF EQUAL
LENGTH.

INDUCTANCE CORE

VIC AMPLITUDE CONTROL
(FIGURE 4-2)

FIGURE 10-3A:VIC DUAL SINGLE-COIL ASS'Y

Voltage Performance Graph (750) of Figure (7-14)

750

INCREASED RESONANT PULSE-FREQUENCY VOLTAGE AMPLITUDE

Vn — WATER FUEL-GAS (70) ON DEMAND

Vc

Vb

Va — AMP INHIBITING PROCESS (690) (Z= R1 + Z2 + Z3 + Re)

RESONAT CAVITY (730) VOLTAGE SURFACES REMAINS CONSTANT

Vo

AMP LEAKAGE ——→

FIGURE 7-14: RESONANT CAVITY WATER-FUEL INJECTION

Figure (10-3B)

LINEAR VOLTAGE WAVE-GUIDE (570A)

POSITIVE ELECTRICAL VOLTAGE SURFACE (66/E9)

DYNAMIC TRAVELING VOLTAGE WAVE-FORM (603)

603a

VOLTAGE PULSE FREQUENCY DIRECTION

WATER GAP (616)

h g f e d c b a

603n

DYNAMIC ELECTRICAL CHARGING EFFECT (612)

OPPOSITE ELECTRICAL STRESS ZONE (RU - RU' ~ ST - ST')

64n
64c
64b
64a

604n

604a

h g f e d c b a

Vo

NEGATIVE ELECTRICAL VOLTAGE SURFACE (67/E10)

WATER SURFACE TENSION (584)

ELECTRICAL CONDUCTANCE ZONE (587) (SKIN EFFECT)

(B) DYNAMIC VOLTAGE STIMULATION

FIGURE 8-1: ELECTRICAL CHARGING STAGE

Voltage Intensifier Circuit (970) of Figure (10-1)

970

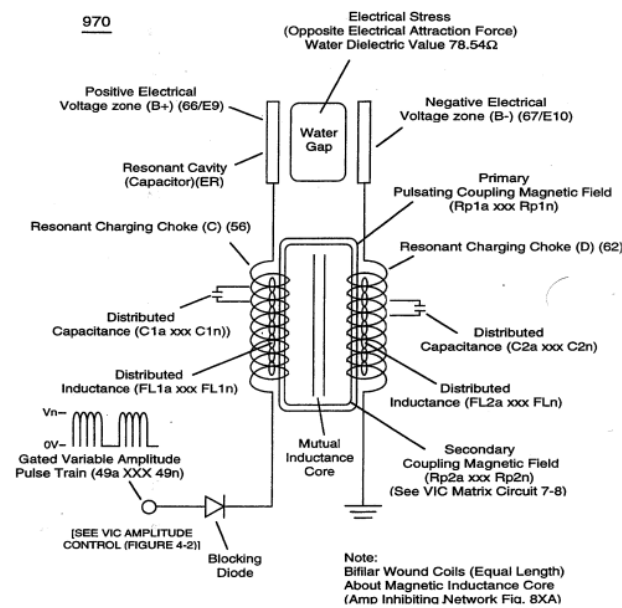Electrical Stress (Opposite Electrical Attraction Force) Water Dielectric Value 78.54Ω

Positive Electrical Voltage zone (B+) (66/E9)

Negative Electrical Voltage zone (B-) (67/E10)

Water Gap

Resonant Cavity (Capacitor)(ER)

Primary Pulsating Coupling Magnetic Field (Rp1a xxx Rp1n)

Resonant Charging Choke (C) (56)

Resonant Charging Choke (D) (62)

Distributed Capacitance (C1a xxx C1n))

Distributed Capacitance (C2a xxx C2n)

Distributed Inductance (FL1a xxx FL1n)

Distributed Inductance (FL2a xxx FLn)

Vn—
0V—
Gated Variable Amplitude Pulse Train (49a XXX 49n)

Mutual Inductance Core

Secondary Coupling Magnetic Field (Rp2a xxx Rp2n) (See VIC Matrix Circuit 7-8)

[SEE VIC AMPLITUDE CONTROL (FIGURE 4-2)]

Blocking Diode

Note: Bifilar Wound Coils (Equal Length) About Magnetic Inductance Core (Amp Inhibiting Network Fig. 8XA)

FIGURE 10-1: VOLTAGE INTENSIFIER CIRCUIT

(620) of figure (7-1)

620

PROGRAMMABLE VARIABLE GATED PULSE - VOLTAGE FREQUENCY (49A XXX 49N)

BLOCKING DIODE

RESONANT CHARGING CHOKE (56) (Z2)

64a

64b

64A XXX 64N

T/3

COIL ORIENTATION

614

EXCITOR ARRAY (ER) (CAPACITOR)

66 / E9

PRIMARY COIL (26)

SECONDARY PICKUP COIL (52) (R1)

67 / E10

622

623

NATURAL WATER DIELECTRIC LIQUID RESISTANCE (Re)

ISOLATED PULSING TRANSFORMER

615

ISOLATED ELECTRICAL GROUND (J)

"TUNED" RESONANT CHARGING CHOKE (62)(Z3)
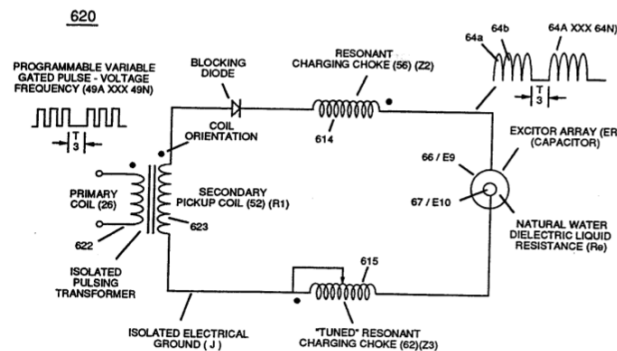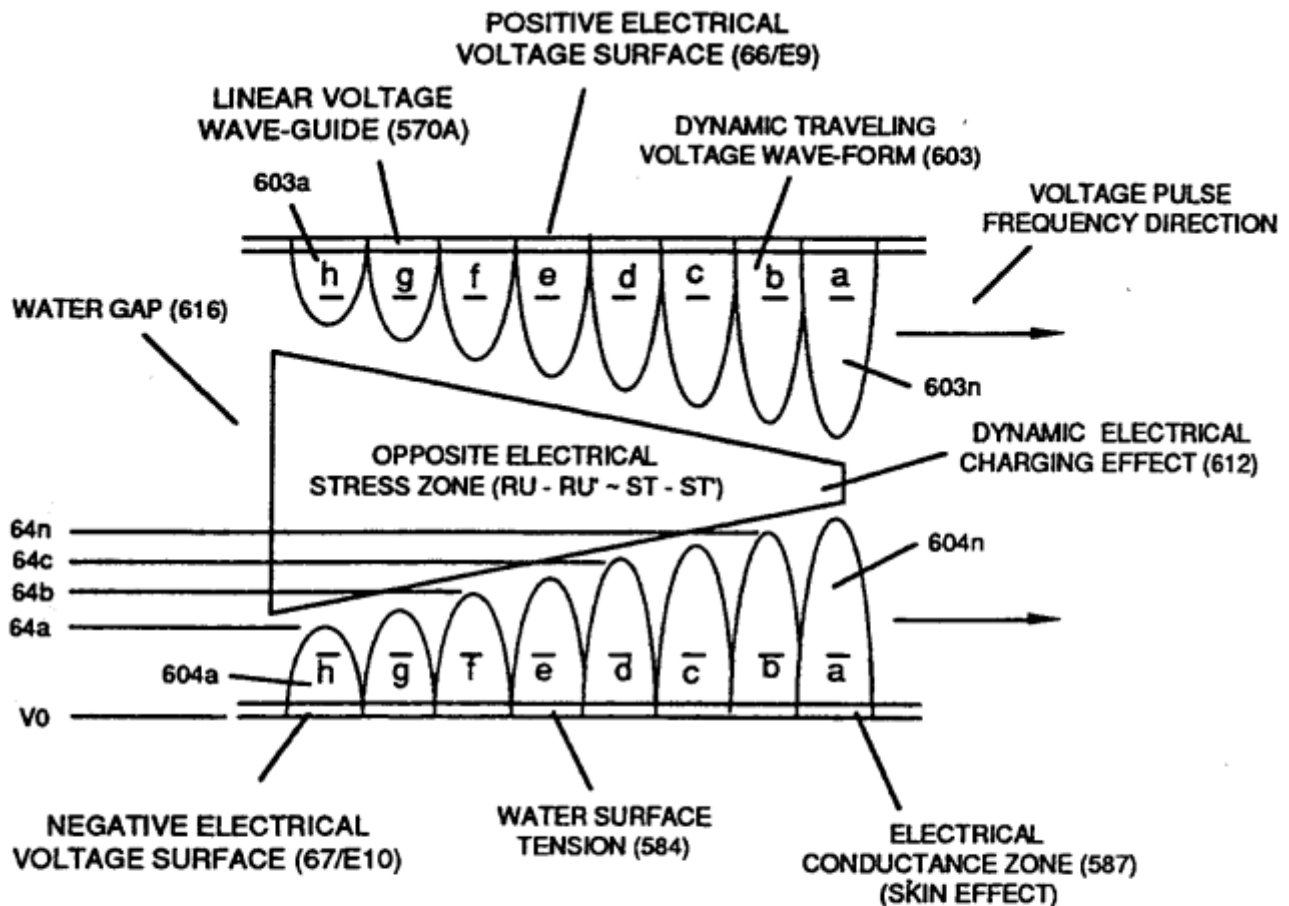
FIGURE 7-1: VIC IMPEDANCE NETWORK

... see **Dynamic Voltage Waveform** (770) of Figure (8-1), once again.

POSITIVE ELECTRICAL
VOLTAGE SURFACE (66/E9)

LINEAR VOLTAGE
WAVE-GUIDE (570A)

DYNAMIC TRAVELING
VOLTAGE WAVE-FORM (603)

603a

VOLTAGE PULSE
FREQUENCY DIRECTION

WATER GAP (616)

603n

DYNAMIC ELECTRICAL
CHARGING EFFECT (612)

OPPOSITE ELECTRICAL
STRESS ZONE (RU - RU' ~ ST - ST')

604n

64n
64c
64b
64a

604a

V0

NEGATIVE ELECTRICAL
VOLTAGE SURFACE (67/E10)

WATER SURFACE
TENSION (584)

ELECTRICAL
CONDUCTANCE ZONE (587)
(SKIN EFFECT)

(B) DYNAMIC VOLTAGE STIMULATION

FIGURE 8-1: ELECTRICAL CHARGING STAGE

In Retrospect, the use of **Stainless Steel** composite coil-wire (430F/FR) consists of both inductance and resistive properties (typically .0048 ohms per foot) which when combined together in metallurgical form aids amp restriction beyond the singularly use of self-inductance magnet (Copper) coil-wire having a lower resistive value.

Stainless Steel bifilar Coil-Stage Assembly (SS56/62a xxx SS56/62n) is electrically placed between **Magnet Coil-Stage Assembly** (56/62a xxx 56/62n) and **Water Gap** (Cp) to obtain optimum **Voltage to Amp Differential Ratio** ($V_{highest}$:A_{lowest} ratio).

Together, **Coil Stages** (56/62a xxx 56/62n + SS56/62a xxx SS56/62) added/stacked sequentially into a single overall coil-array assembly (990A/B) of Figure (10-3) forms

Amp Inhibiting Network (Figure 8XA) as to (970) of Figure (10-1) (hereinafter called **VIC Multi-Coil Spool Assembly**).

> The magnet **Coil-Wire** (56/62) is best suited for **Voltage** inducement while the inductance/capacitance/resistance properties of **Stainless Steel coil-wire** (SS56-SS62) is appropriately used to **restrict electron movement** beyond the self-inductance of each energized coil when elevated voltage levels *(up to beyond 40 kilovolts)* are to be reached/obtained without experiencing any appreciable amount of "**Amp Influxing**."

Generally, <u>magnet coil-wire length is longer</u> than the <u>Stainless steel coil-wire length</u> and magnet bifilar-coil (56/62) is placed on top of **Stainless Steel bifilar-coil** (SS56/62) to maximize mutual inductance coil-field (Rp2) (adding Rp1+Rp2) of (690) of Figure (7-8) to cause coil capacitance (Cda xxx Cdn) to help maintain and even increase pulse voltage amplitude (xxx $V_n + V_{n1} + V_{n2} + V_n$ .... etc.) while the resistive value (Rs2) of SS Coil-Wire (SS56/62) performs the work of further resisting the flow of amps not inhibited by both self-Inductance fields (Rpl + Rp2), as so illustrated in (690) of Figure (7-8).
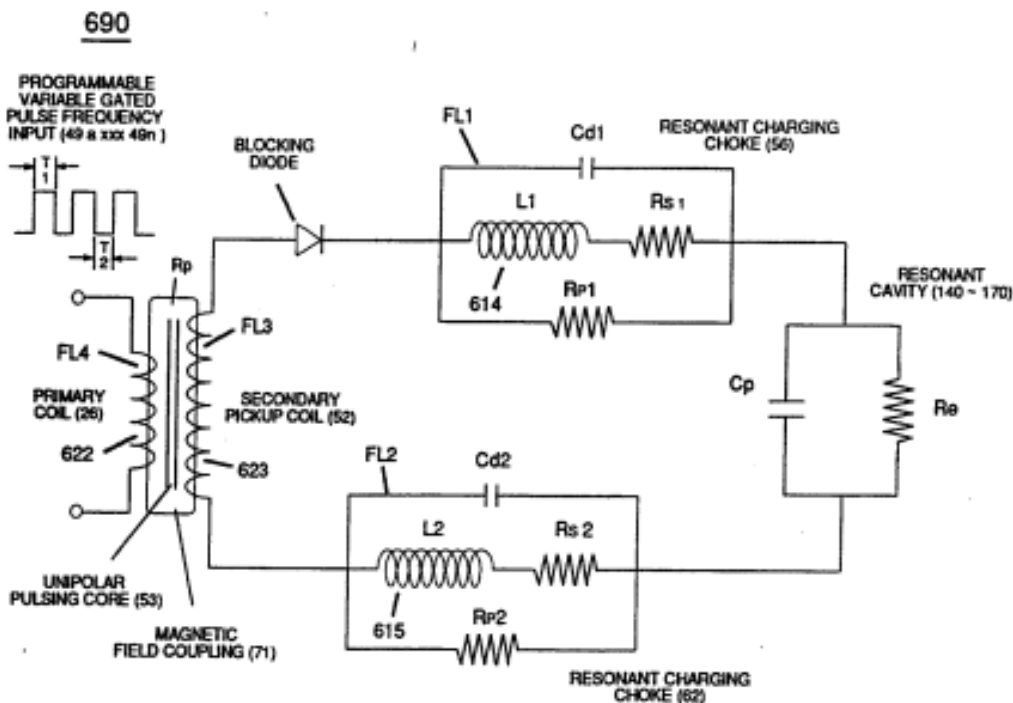

(690) of Figure (7-8)

FIGURE 7-8: VIC MATRIX CIRCUIT

> In all cases, bifilar coils (56/62 - SS56/62) are electromagnetically orientated **in the same direction**.

> In terms of operability, electrically flexing (**Particle Oscillation**) the combustible atoms of the water molecule as a "**Energy Generator**" by way of opposite voltage polarity is extremely economical since voltage is not consumed in an electronic circuit.
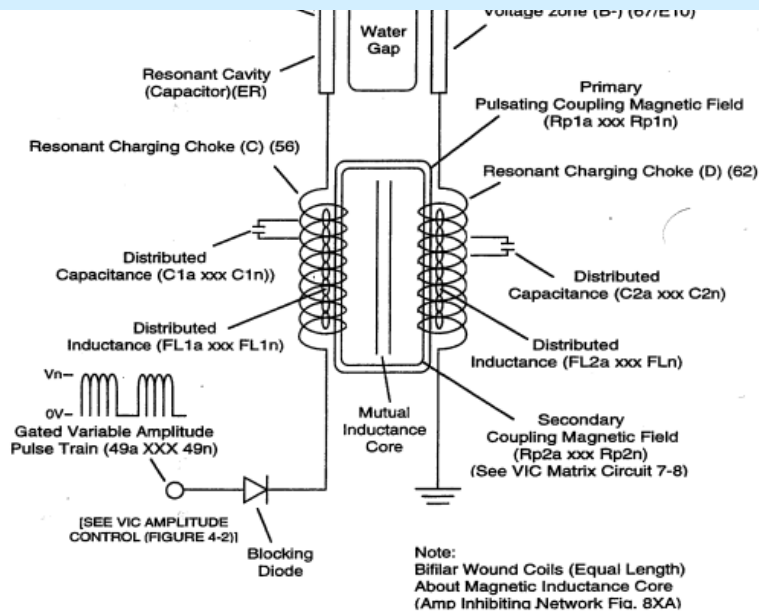
FIGURE 10-1: VOLTAGE INTENSIFIER CIRCUIT

Amp Inhibiting Circuit (970) of

Figure (10-1) restricts/inhibits amp flow to a minimal level while elevating "**Difference of Potential**" to the highest possible level.

The greater the "**Difference of Potential**" (in this case, electrical stress) the greater amount of work is performed

... thereby, being in compliance with the **Laws of Physics** since atoms are the source of all energy in our physical universe and atoms are directly responsive to / stimulated by external electrical forces.